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PILOT PRODUCTION OF GLASS CRYSTAL HOLDERS

HC-(XM-2)/U; HC-(XM-3)/U; HC-(XM-4)/U

FINAL REPORT: MAY 1958 THROUGH SEPTEMBER 1962

CONTRACT NO.: DA - 36 - 039 - \$C - 81 255

ORDER NO.:

43810-PP-58-81-81

PLACED BY:

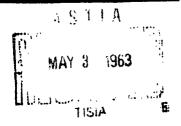
(U.S. ARMY SIGNAL SUPPLY AGENCY), PHILADELPHIA, PA.

NOW CALLED:

U.S. ARMY ELECTRONIC MATERIAL AGENCY

CONTRACTOR:

CORNING GLASS WORKS, CORNING, N.Y.



CORNING CORNING CORNING GLASS WORKS

CORNING GLASS WORKS
Corning, New York

PILOT PRODUCTION OF GLASS CRYSTAL HOLDERS

HC-(XM-2)/U; HC-(XM-3)/U; HC-(XM-4)/U

FINAL REPORT: MAY 1958 THROUGH SEPTEMBER 1962

CONTRACT NUMBER: DA-36-039-SC-81255

ORDER NUMBER: 43810-PP-58-81-81

PLACED BY: (UNITED STATES ARMY SIGNAL SUPPLY AGENCY) NOW CALLED: UNITED STATES ARMY ELECTRONIC MATERIEL AGENCY PHILADELPHIA, PENNSYLVANIA

> CONTRACTOR: CORNING GLASS WORKS CORNING, NEW YORK

REPORT PREPARED BY: R. K. WHITNEY

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I. ABSTRACT

A review of requirements, dimensions, and materials is presented with the resultant specification for glass holders. Fundamental glass properties and sealing characteristics are presented. Description of sealing equipment used, plus the process procedures gone through during the preparation of pre-production samples is described. A review of major steps taken for each glass crystal holder is made.

I. ABSTRACT

A review of requirements, dimensions, and materials is presented with the resultant specification for glass holders. Fundamental glass properties and sealing characteristics are presented. Description of sealing equipment used, plus the process procedures gone through during the preparation of pre-production samples is described. A review of major steps taken for each glass crystal holder is made.

2. PURPOSE

The purpose of the work done under the subject contract was to perform Steps I and II of Industrial Preparedness for three crystal holders, HC-(XM-2)/U; HC-(XM-3)/U; and HC-(XM-4)/U. In addition, sealing performance of the holder parts in question was to be demonstrated.

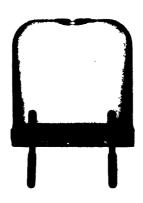
3. CRYSTAL HOLDER NOMENCLATURE

So that all readers of this report are on common ground, a cross reference is given for various types of crystal holders with similar form factors:

Metal Holder	Experimental Glass Holder	Glass Holder	Corning Glass Work For Glass Hold	•
HC-6/U	HC-(XM-2)/U	HC-27/U	Bulb: T6-BIC; Cod Base: Cod	e 131270 e 131275
HC-13/U	HO-(XM-3)/U	HC -2 8/U	Bulb: T6-CIC; Code Base: Code	e 131280 e 131285
HO-18/U	HC-(XM-4)/U	HC-26/U	Bulb: T3-RIC; Cod Base: Cod	• 131260 • 131265
HC -2 5/U	-	HO-29/U	Bulb: T3-RIC; Cod Base: Not Designa	

CRYSTAL HOLDER

HC-(XM-2)/U OR HC-27/U



CORNING GLASS WORKS

PARTS DESIGNATION

Bulb T6-BlC Code 131270

Base .728" Long, .321" Wide With Two Leads .430" Long Code 131275







CORNING GLASS WORKS

Product Engineering Receiver Bulb Sales Dept. Corning, New York

Date 3/15/62 Product Specification

131270 Code

Bulb, T6-BIC

Supersedes 10/3/60 Page 1 Bulb For Crystal Holder HC-27/U

Glass: 7052

Finish: Mold blown, open end diamond saw cut, glazed, and annealed

<u>Visual Inspection</u>: Standard 7052 tubing inspection, except as noted:

3.1. Scale: Reject all degrees.

3.2. Stones: Maximum acceptable 1/32" greatest dimension, or two or more where area does not exceed one stone 1/32" square well buried. Reject all degrees in area 3/32" from cut edge.

3.3. Knots: Maximum acceptable 1/32" greatest dimension, or two or more where area does not exceed one knot 1/32" square well buried. Reject all degrees in area 3/32" from cut edge.

3.4. Chips: Reject all degrees on bulb top and on side more than 3/32" from cut edge. Fine grinding or cutting chips permitted, less than 3/32" from cut edge. Maximum acceptable on side of bulb, one that does not reduce wall below minimum dimensions and is less than 1/32" in greatest dimension. No chips are allowed at cut edge that exceed one-third wall thickness of bulb in question.

3.5. Adhered Glass: Reject all degrees.

3.6. Dirty Bulb: Reject all degrees inside and outside. Bulbs shall be free of glass dust, dirt, grease, and any foreign material.

3.7. Scuff Or Scratch: Reject bulb if a single scratch exceeds one-half of the bulb periphery. Reject bulb if two or more scratches or scuffs exceeds one-quarter of the bulb periphery.

3.8. Blister And/Or Seed: Reject all open blisters or seeds. Reject all blisters or seeds with maximum dimension greater than 1/64".

Reject all open airlines. Reject all airlines greater than 3.9. Airline: 1/64" wide.

Reject bulb if cord exceeds one-quarter of the periphery. Reject <u>Coca:</u> fricut edge. all degrees in arm

3.11. Checks And Cracks: Reject all degrees.

3.12. Slack Blown: Reject all degrees.

4. <u>Dimensions</u>: See drawing and notes.

1575 R. ±.005 3/5 ZONE ±,005 1575R ₩ONE "B" 1575 R. ,705 ±,004 576 ZONE "A WITHIN . 010 SQUARE FIRE POLISH OPEN END

Wall Thickness Notes:

Wall .035-.045 desired throughout.

2. Limits:

Zone A: .027-.043 Zone B: .020-.045

(Center closed

end)

.011-.035 Zone C:

> (Corner radius closed end)

*Chanae **Addition ***Deletion

- 7 -

Scale:

PC No.

All Dimensions in Inches. Dimensions shown without tolerance are design centers.

Date 1/11/62 Code 131275 Product Specification Base .728 Long, .321 Wide With Two Leads .430 Long

Supersedes 6/7/61 Page 1 of 3
Base For Crystal Holder HC-27/U

I. Material: Glass: 7052 clear

Metal: Kovar or equal

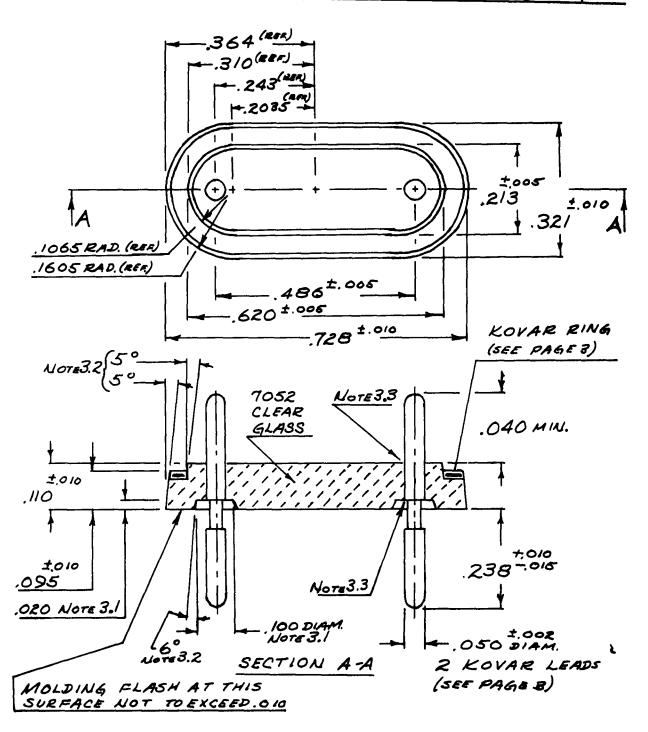
2. Finish: Molded finish

- 3. <u>Dimensions</u>: See drawings on Pages 2 and 3, plus following notes:
 - 3.1. Recess required, but dimensions not controlled and are for reference only.
 - 3.2. Draft is optional.
 - 3.3. At either surface through which pins emerge from the main body of the base, glass meniscus shall not extend on the pins more than .025. Meniscus check or crack shall not be rejectable.
 - 3.4. When Kovar ring is specified to be glazed, this glaze shall completely surround the ring, leaving no bare metal exposed. This ring shall be securely sealed all around its perimeter to the main body of the base glass.



Date 1/11/62 Code 131275 Product Specification Base .728 Long, .321 Wide With Two Leads .430 Long

Supersedes 6/7/61 Page 2



*Change **Addition

-9 -

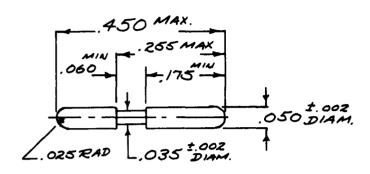
PC No. R8-690

***Deletion Scale: 5X All Dimensions in Inches. Dimensions shown without tolerance are design centers.

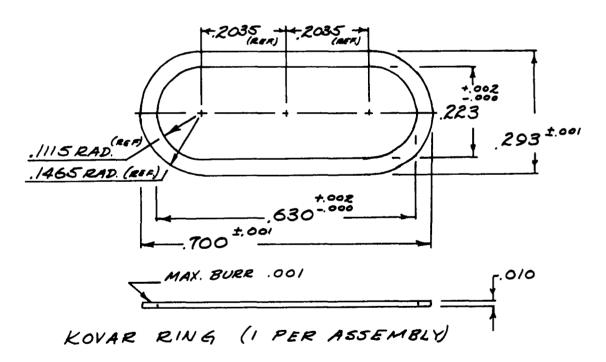


Date 1/11/62 Code 131275 Product Specification Base .728 Long, .321 Wide With Two Leads .430 Long

Supersedes 6/7/61 Page 3 of 3



KOVAR LEAD (2 PER ASSEMBLY)



THICKNESS AFTER GLAZING ALL OVER WITH 7052 GLASS -. 020 \$.005, SEE NOTE 3.4

*Change **Addition ***Deletion

- 10 -

Scale: 5X

PC No. RB-690

All Dimensions in Inches. Dimensions shown without tolerance are design centers.

CRYSTAL HOLDER

HC-(XM-3)/U OR HC-28/U



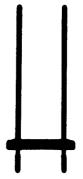
CORNING GLASS WORKS

PARTS DESIGNATION

Bulb T6-C1C Code 131280

Base .728" Long, .32" Wide With Two Leads 1.710" Long Code 131285





Coming, New York

Date 3/15/62 Co Product Specification Bulb, T6-CIC

Code 131280

Supersedes 10/3/60 Page 1 of 2
Bulb For Holder HC-28/1

1. Glass: 7052

2. Finish: Mold blown, open end diamond saw cut, glazed, and annealed

3. <u>Visual Inspection</u>: Standard 7052 tubing inspection per Master Specification EPS-9, except as noted:

3.1. Scale: Reject all degrees.

3.2. Stones: Maximum acceptable 1/32" greatest dimension, or two or more where area does not exceed one stone 1/32" square well buried. Reject all degrees in area 3/32" from cut edge.

3.3. <u>Knots</u>: Maximum acceptable 1/32" greatest dimension, or two or more where area does not exceed one knot 1/32" square well buried. Reject all degrees in area 3/32" from cut edge.

3.4. Chips: Reject all degrees on bulb top and on side more than 3/32" from cut edge. Fine grinding or cutting chips permitted, less than 3/32" from cut edge. Maximum acceptable on side of bulb, one that does not reduce wall below minimum dimensions and is less than 1/32" in greatest dimension. No chips are allowed at cut edge that exceed one—third wall thickness of bulb in question.

3.5. Adhered Glass: Reject all degrees.

3.6. <u>Dirty Bulb</u>: Reject all degrees inside and outside. Bulbs shall be free of glass dust, dirt, grease, and any foreign material.

3.7. <u>Scuff Or Scratch</u>: Reject bulb if a single scratch exceeds one-half of the bulb periphery. Reject bulb if two or more scratches or scuffs exceed one-quarter of the bulb periphery.

3.8. <u>Blister And/Or Seed</u>: Reject all open blisters or seeds. Reject all blisters or seeds with maximum dimension greater than 1/64".

3.9. <u>Airline</u>: Reject all open airlines. Reject all airlines greater than 1/64" wide.

3.10. <u>Cord</u>: Reject bulb if cord exceeds one-quarter of the periphery. Reject all degrees in area 3/32" from cut edge.

3.11. Checks And Cracks: Reject all degrees.

3.12. Siack Blown: Reject all degrees.

*Change **Addition ***Deletion

- 12 -

All Dimensions in Inches. Dimensions shown without tolerance are design centers.

Date 3/15/62 Product Specification Bulb, T6-CIC

Code 131280

of 2

Supersedes 10/3/60 Page 2

Wali Thickness Notes:

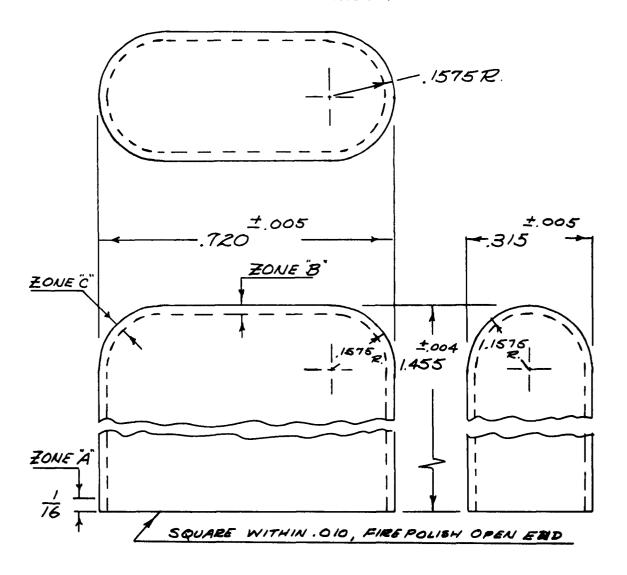
1. Wall .035-.045 desired throughout.

2. Limits:

Zone A: .027-.043

Zone B: .020-.045 (Center closed end)

Zone C: .011-.035 (Corner radius closed end)



*Change **Addition

- 13 -

***Deletion

Scale: 5X

PC No. RB-750 All Dimensions in Inches. Dimensions shown without tolerance are design centers.

Date 3/15/62 Code 131285 Product Specification Base .728 Long, .321 Wide With Two Leads 1.710 Long

Supersedes 1/11/62 Page 1 of 3
Base For Crystal Holder HC-28/U

I. Material: Glass: 7052 clear

Corning, New York

Metal: Kovar or equal

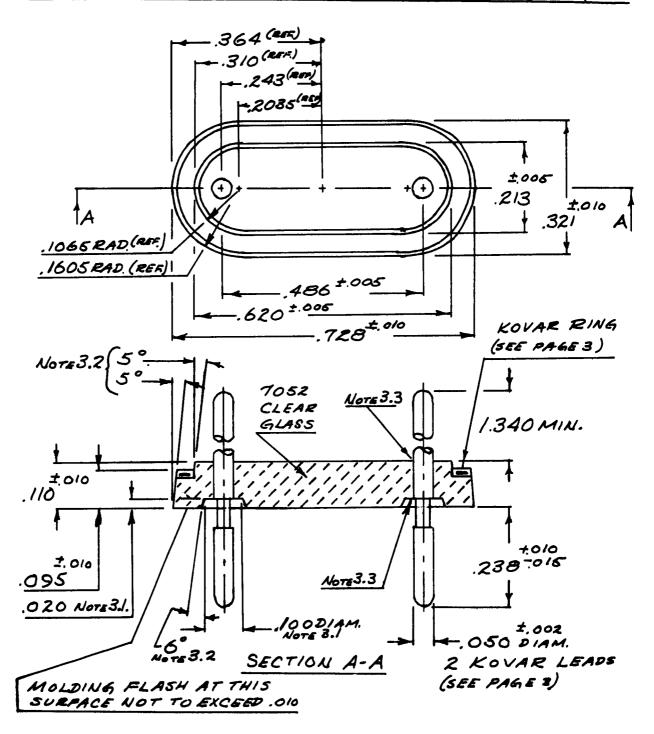
2. Finish: Molded finish

- 3. <u>Dimensions</u>: See drawings on Pages 2 and 3, plus following notes:
 - 3.1. Recess required, but dimensions not controlled and are for reference only.
 - 3.2. Draft is optional.
 - 3.3. At either surface through which pins emerge from the main body of the base, glass meniscus shall not extend on the pins more than .025. Meniscus check or crack shall not be rejectable.
 - 3.4. When Kovar ring is specified to be glazed, this glaze shall completely surround the ring, leaving no bare metal exposed. The ring shall be securely sealed all around its perimeter to the main body of the base glass.



Date 3/15/62 Code 131285 Product Specification Base .728 Long, .321 Wide With Two Leads 1.710 Long

Supersedes 1/11/62 Page 2 of 3



**Addition
***Deletion

- 15 -

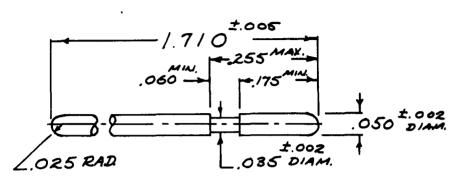
All Dimensions in Inches. Dimensions shown without tolerance are design centers.



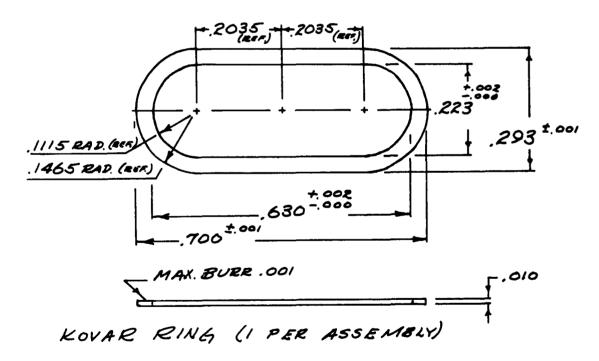
Corning, New York

Date 3/15/62 Cede 131285 Product Specification
Base .728 Long, .321 Wide With Two Leads 1.710 Long

Supersedes 1/11/62 Page 3 of 3



KOVAR LEAD (2 PER ASSEMBLY)



THICKNESS AFTER GLAZING ALL OVER WITH 7052 GLASS - .020 ±.005, SEE NOTE 3.4

*Change **Addition

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***Deletion Scale: 5X

PC No. RB-749

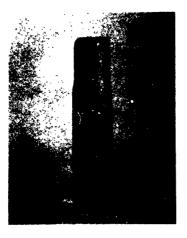
All Dimensions in Inches. Dimensions shown without tolerance are design centers.

C R Y S T A L H O L D E R HC-(XM-4)/U OR HC-26/U



CORNING GLASS WORKS
PARTS DESIGNATION

Bulb T3-R1C Code 131260



Base .365" Long, .098" Wide With Two Leads 1.730" Long Code 131265



Corning, New York

Date 3/15/62 Product Specification Code 131260

Bulb, T3-RIC

Supersedes 10/4/60 Page 1 of 2
Bulb For Crystal Holder HC-25/U

1. Glass: 7052

HC-25/U

- 2. Finish: Mold blown, open end cut, glazed, and annealed
- 3. <u>Visual Inspection</u>: Standard 7052 tubing inspection, except as noted:
 - 3.1. <u>Scale</u>: Reject all degrees.
 - 3.2. Stones: Maximum acceptable 1/32" greatest dimension, or two or more where area does not exceed one stone 1/32" square well buried. Reject all degrees in area 3/16" from cut edge and in Zone A.
 - 3.3. <u>Knots</u>: Maximum acceptable 1/32" greatest dimension, or two or more where area does not exceed one knot 1/32" square well buried. Reject all degrees in area 3/16" from cut edge and in Zone A.
 - 3.4. Chips: Reject all degrees on bulb top and on side more than 3/32" from cut edge. Fine grinding or cutting chips permitted, less than 3/32" from cut edge. Maximum acceptable on side of bulb, one that does not reduce wall below minimum dimensions and is less than 1/32" in greatest dimension. No chips are allowed at cut edge that exceed one-third wall thickness of bulb in question.
 - 3.5. Adhered Glass: Reject all degrees.
 - 3.6. <u>Dirty Bulb</u>: Reject all degrees inside and outside. Bulbs shall be free of glass dust, dirt, grease, and any foreign material.
 - 3.7. <u>Scuff Or Scratch</u>: Reject bulb if a single scratch exceeds one-half of the bulb periphery. Reject bulb if two or more scratches or scuffs exceed one-quarter of the bulb periphery.
 - 3.8. <u>Blister And/Or Seed</u>: Reject all open blisters or seeds. Reject all blisters or seeds with maximum dimension greater than 1/64".
 - 3.9. <u>Airline</u>: Reject all open airlines. Reject all airlines greater than 1/64" wide.
 - 3.10. <u>Cord</u>: Reject builb if cord exceeds one-quarter of the periphery. Reject all degrees in Zone A.
 - 3.11. Checks And Cracks: Reject all degrees.
 - 3.12. Slack Blown: Reject all degrees.

*Change **Addition ***Deletion



Date 3/15/62 **Product Specification**

Code 131260

Bulb, T3-RIC

Supersedes 10/4/60 Page 2

Wall Thickness Notes:

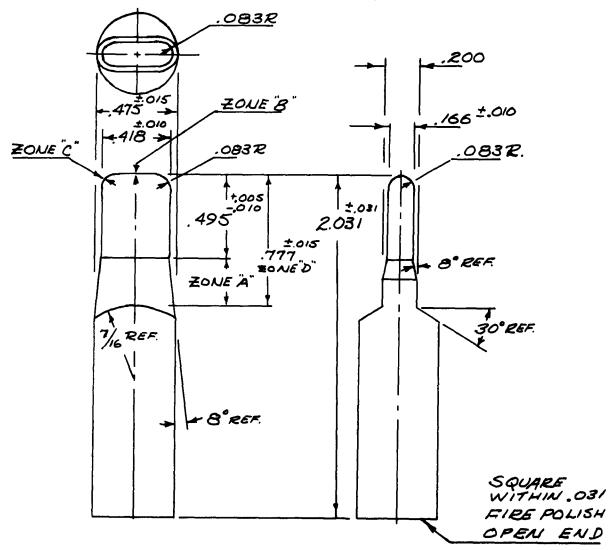
Wall .022-.028 desired throughout Zone D.

2. Limits:

Zone A: .017-.033

Zone B: .030-.045 (Center closed end)

.010-.040 (Corner radius of closed end) Zone C:





CORNING GLASS WORKS

Product Engineering Receiver Bulb Sales Dept. Corning, New York

Date 1/11/62 Code 131265 Product Specification

Base .365 Long, .098 Wide With Two Leads 1.730 Long

Supersedes 6/7/61 Page ! Base For Crystal Holder HC-25/U

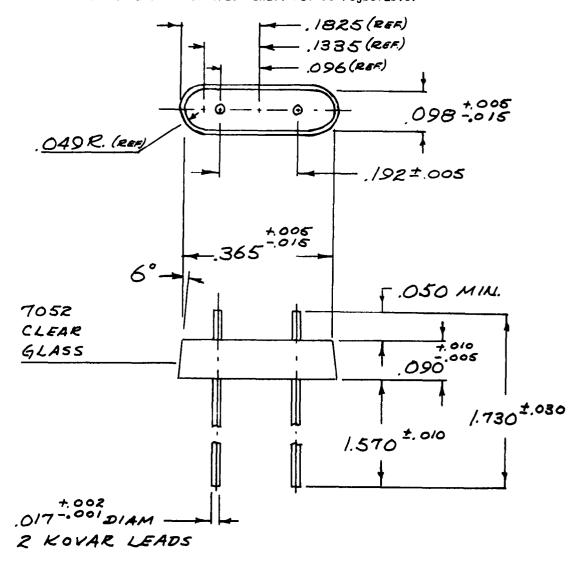
I. Material: Glass: 7052 clear

Metal: Kovar or equal

2. Finish: Molded finish

3. <u>Dimensions</u>: See drawing on Page !, plus following note:

3.1. At either surface through which leads emerge from the main body of the base, glass meniscus shall not extend on the leads more than .025. Meniscus check or crack shall not be rejectable.



*Change **Addition ***Deletion

- 20 -

Scale: 5X

PC No. RB-689

All Dimensions in Inches. Dimensions shown without tolerance are design centers.

4. STATEMENT OF PROBLEM AND PLANNED APPROACH

This report will describe procedures and techniques for sealing together bulbs (covers) and bases of glass crystal holders.

Detailed production processing information for bulbs and bases is specifically excluded as a part of this contract's work.

The detailed requirements for the glass crystal holders covered in this work are described for the reader's reference.

- 4.1. The glass crystal holders are to meet the applicable requirements of MIL-H-10056B. In addition, the following requirements are to be met.
 - 4.1.1. Crystal units sealed in these glass holders shall give equivalent performance to crystal units soldered in the regular metal holders when tested in accordance with MLL-C-3098B.
 - 4.1.2. The glass shall be clean and contain no bubbles greater than 1/8". There shall be no loosening of pins for the base, and the glass shall contain no radial or other detrimental cracks when examined as specified in Paragraph 4.6.1.1. of MIL-H-10056B.
 - 4.1.3. The sealed crystal holder shall be placed on a grounded metal plate and the electrode of a Tesla coil placed across both pins. The

4.1. (Continued)

4.1.3. (Continued)

Tesla coil shall be energized. After a period of forty-eight hours, the test shall be repeated. When tested in this fashion, the presence of a light blue glow discharge which fills the holder shall be taken as evidence of a vacuum. After the forty-eight hour period, there shall be no evidence of leakage. A purplish blue glow discharge, restricted in area, or a spark discharge shall be considered as evidence of leakage.

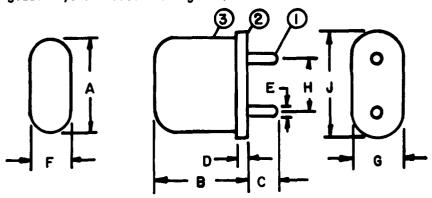
(Such a test may be detrimental to the plating on a quartz crystal.)

4.1.4. The HO-(XM-2)/U and HO-(XM-3)/U holders shall sustain a load of thirty pounds along the axis of the pins; the HC-(XM-4)/U holder shall sustain a load of ten pounds along the axis of the pins. These loads are to be applied according to Paragraph 4.6.4. of MIL-H-10056B. When tested as described, the glass shall show no evidence of loosening from the pins or separation of the base from the cover at the base seal.

- 4. STATEMENT OF PROBLEM AND PLANNED APPROACH (Continued)
 - 4.1. (Continued)
 - 4.1.5. The sealed glass holder shall be held at a temperature of -55° C. for ten minutes and immediately immersed in boiling water. There shall be no evidence of cracking, breaking, or leakage.
 - 4.1.6. Sealing of pre-production samples of the crystal holders is to be accomplished on sealing equipment owned by the United States Government (or equivalent equipment). The crystal holder is to be evacuated and the sealing shall be accomplished without raising the crystal to a temperature exceeding 250° C. (This stipulation was modified)

This sealing equipment was purchased by the Government from Philips Electronics Industries, Limited, in Toronto, Ontario, Canada.

4.2. The specified dimensions and materials of these three glass crystal holders are given.



	Holder Type					
<u>Dimension</u>	HC-(XM-2)/U	HC-(XM-3)/U	HC-(XM-4)/U			
A	.720 ± .005	.720 ± .005	.418 ± .010			
В	.765 ± .010	1.516 ± .010	.515 + .010 015			
С	.238 + .010 015	.238 + .010 015	1.500 Minimum			
D	.065 ± .010	.065 ± .010	Not Specified			
E	.050 ± .002	.050 ± .002	.017 + .002 001			
F	.315 ± .005	.315 ± .005	.166 ± .010			
G	.345 + .000	.345 + .000 005	.166 ± .010			
н	.486 ± .008	.486 ± .008	.192 ± .008			
J	.750 + .000 005	.750 + .000 005	.418 ± .010			

4 2. (Continued)

Notes:

- I. All dimensions in inches.
- 2. Item No. I shall project .040 inches above the inside glass seal for HC-(XM-2)/U and HC-(XM-4)/U and I.340 inches for HC-(XM-3)/U.
- Thickness of glass of bulb (cover) is described in detail in Corning part specifications.

Ltem	Number	<u>Description</u>	<u>Material</u>	Quantity
	1	Pin (Lead)	Kovar ^(R) or equal	2
	2	Base	7052 glass	ŀ
(R)	3	Bulb (Cover)	7052 glass	I
	Register Corporat		Westinghouse Elec	tric

The dimensions and tolerances originally specified by the United States Government were identical to those specified for similar metal holders. The tolerances and dimensions listed above were agreeably modified to provide compatibility with glass working techniques which are indeed different from metal working techniques. The glass holder's finished form factor, in the area where bulb and base are sealed, will be distorted from that depicted in the outline drawing.

4.3. The materials to be used are Corning's PYREX Brand 7052 Glass and Kovar Alloy. These are the materials that were used by Philips Electronics Industries, Limited (previously called Canadian Radio Manufacturing Corporation, Limited) of Toronto, Ontario, Canada, for their glass crystal holders designated RG-1 and RG-2. These two holders are similar to the HC-(XM-2)/U and HC-(XM-4)/U holders respectively. In view of the stringent requirements noted above, in particular the severe thermal shock test, low thermal expansion materials are required for these holders. Lower thermal expansion materials are available, but sealing and annealing conditions, plus compatibility with a 250° C. desired maximum quartz temperature, indicate that the 7052 Glass and Kovar combination is an optimum choice of materials.

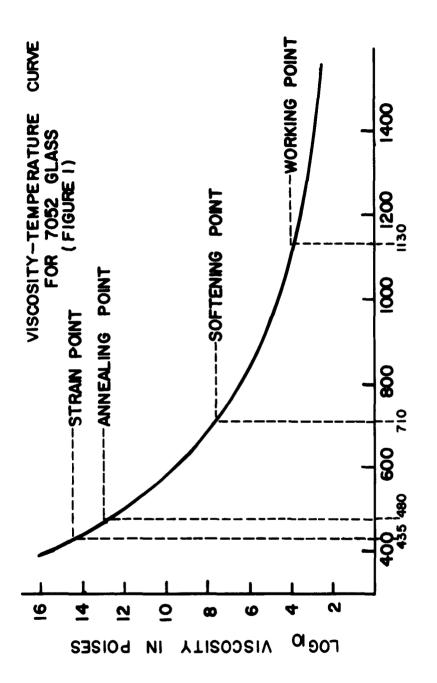
4.4. The approach for completion of the work was planned along conventional lines: Design glass parts that are compatible with sealing equipment and specified dimensions; dimensionally test these parts by actually sealing experimentation; subject sealed holders to preproduction tests; and produce pilot run quantities. Corning Glass Works would produce the bulbs; bases would be obtained from a subcontractor - L. L. Constantin, Lodi, New Jersey; sealing would be done at Scientific Radio Products, Inc., Loveland, Colorado, and McCoy Electronics Company, Mount Holly Springs, Pennsylvania.

5. GLASS WORKING AND SEALING

5.1. Glass is a noncrystalline material that has no regular internal structure. It is rigid at ordinary temperatures and soft or almost fluid at high temperatures. It has no definite freezing point.

At ordinary temperatures the viscosity of glass is so high that it can be considered to be infinite. As the temperature is raised, however, the viscosity decreases and the glass gradually assumes the character of a liquid. Four points on the viscosity-temperature curve have been arbitrarily chosen to represent the softness of the glass at important points in its change from solid to liquid. Figure I is a viscosity-temperature curve for 7052 glass.

The following definitions for strain, annealing and softening points are taken from those tentatively adopted by the American Society For Testing Materials; that for Working Point is employed by Corning Glass Works and corresponds to the upper end of the working range as defined by the American Society For Testing Materials.



TEMPERATURE, °C

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5.1. (Continued)

Strain Point

The temperature at the lower end of the annealing range, at which the internal stress is substantially relieved in four hours. The strain point corresponds to a viscosity of $10^{14.50}$ poises when measured by the Tentative Method Of Test For Annealing Point And Strain Point Of Glass (A.S.T.M. Designation: C. 336). The strain point for 7052 glass is 435° C.

Annealing Point

The temperature at the upper end of the annealing range, at which the internal stress is substantially relieved in fifteen minutes. The annealing point corresponds to a viscosity of $10^{13.00}$ poises when measured by the Tentative Method Of Test For Annealing Point And Strain Point Of Glass (A.S.T.M. Designation: C. 336). The annealing point for 7052 glass is 480° C.

In an annealing operation the glass is heated somewhat above the annealing point and slowly cooled to somewhat below the strain point. Deformation of the glass can become a problem about 50° C. above the annealing point.

5.1. (Continued)

Softening Point

The temperature at which a uniform fiber, 0.55 to 0.75 mm in diameter and 23.5 cm. in length, elongates under its own weight at a rate of 1 mm per minute when the upper 10 cm of its length is heated in the manner prescribed in the Tentative Method Of Test For Softening Point Of Glass (A.S.T.M. Designation: C. 338) at a rate of approximately 5° C. per minute. For glass of density near 2.5 gm./cm. 3 this temperature corresponds to a viscosity of $10^{7.6}$ poises. The softening point for 7052 glass is 710° C.

At the softening point the glass deforms very rapidly and starts to adhere to other bodies.

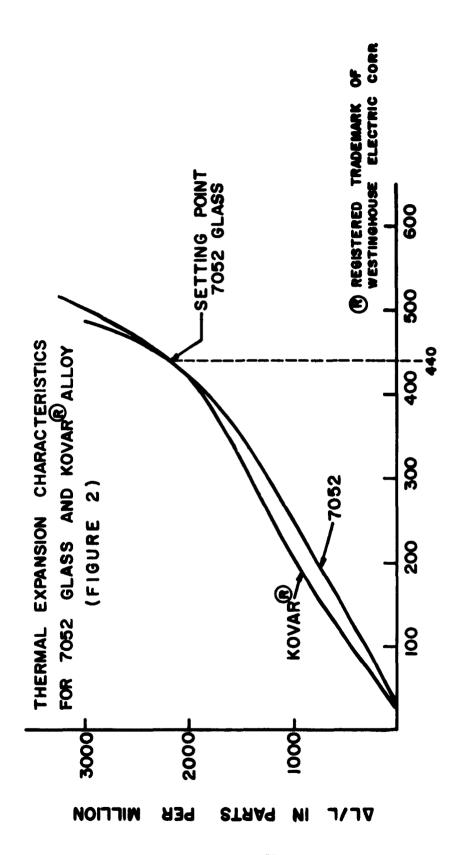
Working Point

The temperature where the glass is soft enough for hot working by most of the common methods. Viscosity at the working point is 10^4 poises. The working point for 7052 glass is 1130° C.

5.1. (Continued)

As the temperature is raised, glasses tend to expand. In general the change is smaller than with most ordinary substances, but because of the nature of glass the expansion is often quite important, both in connection with heat shock resistance and in connection with rigid seals to other materials such as metals, ceramics and other glasses.

Figure 2 shows "expansion curves" for 7052 glass and Kovar alloy in which the change in length per unit length $(\Delta L/L)$ is plotted against the temperature (T) in degrees centigrade. Actually this should be called an elongation curve since the quantity plotted against temperature is the specific elongation and not the expansion coefficient. It will be noted that the curve is initially linear but that it swings upward, indicating a higher rate of expansion, as the annealing zone is approached. The quantity which is usually referred to by the term "expansion", actually "Thermal Expansion Coefficient", is the slope of the initial, linear portion of this curve. To be more precise, it is the average change of length per unit length per degree C. between 0° C. and 300° C. This figure gives a good indication of the ability of the glass to withstand thermal shock.



TEMPERATURE, °C

5.1. (Continued)

For sealing applications, values are often given for the average expansion coefficient from room temperature to the setting point. The setting point is arbitrarily defined as that point on the viscosity-temperature curve that is 5° C. above the strain point. A comparison of the expansion coefficients to the setting point between a material of known expansion and a particular glass will give a good estimate of sealing compatibility. However, for precise predictions of residual sealing stresses due to expansion differences, complete expansion curves for the sealing materials should be consulted.

The thermal expansion coefficient of 7052 glass between 0° - 300° C. is $46 \times 10^{-7}/^{\circ}$ C. The thermal expansion coefficient of 7052 glass from room temperature to the setting point is $53 \times 10^{-7}/^{\circ}$ C.

The thermal expansion differential between Kovar and 7052 glass at the setting point of 7052 (440° C.) is twenty parts per million. In general, this low a value is interpreted as a very good sealing condition.

5.2. When properly fabricated parts for the three crystal holders are sealed together, glass-to-glass seals are made. Whenever glass seals are made, it is essential that the glass be "worked". "Working" means that movement of the glass must occur so that the two adjacent glass members are intimately intermingled. Glass-to-glass seals are influenced by three factors: time, temperature, and the amount of working. In making a seal of the type required for these crystal holders, the amount of seal working is restricted by physical and mechanical limitations. Furthermore, time and temperature must be controlled so that heat transfer to the plated quartz blank is minimized. The success of a glass seal is also a function of the rate of cooling between the annealing point and the strain point of the glass. At a high rate of cooling, a permanent stress may be left which may cause failure later.

With these limitations and factors in mind, the discussion is now directed towards crystal holders.

These principles will apply regardless of what sealing equipment is used. An understanding of the principles will only aid in making better seals. Accordingly, this section will not deal with the equipment used, but with the sealing process.

5.2. (Continued)

The minimum temperature at which 7052 glass can be sealed and still provide the proper glass flow to prevent re-entrant angles is in the 825° C. to 900° C. region.

The seal area at this temperature is bright cherry red to orange in color.

All the specific temperatures that are involved in this seal system are listed:

250° C. - Desired maximum quartz limit

435° C. - Strain Point, 7052 Glass

480° C. - Annealing Point, 7052 Glass

710° C. - Softening Point, 7052 Glass

840° C. - Approximate sealing temperature in this system (See Section 5.4.2.4.)

Achievement and maintenance of these temperatures at the proper time in the seling cycle requires good control of the operation. From a purely theoretical standpoint, the sealing system for these crystal holders is one which is filled with compromises.

The seal area cannot be raised to a temperature as high as might be desired. This limitation means that the glass parts must be of sufficient accuracy and fit with one another so that when heated to the minimum temperature of approximately 825° C., sufficient flow will occur.

5.2. (Continued)

The physical arrangement of the sealing equipment and the parts to be sealed do not provide a means of working the seal area as thoroughly as might be desired. As in the preceding paragraph, glass part accuracy and alignment must maximize the amount of working possible so that, coupled with the 825° C, temperature, smooth transitions from one glass member to the other glass member are achieved. Without proper fillets and smooth transitions, sharp re-entrant angles will be left in the seal area.

The actual temperature of the seal area must be cooled at a rate, through the annealing range of the glass (from above 480° C. to below 435° C,) that is sufficiently slow to relieve stresses introduced during sealing. These stresses, if not relieved, may be the source of subsequent failures. In normal glass working practices, the best annealing is done as a separate operation in which the whole article is carried through a complete annealing cycle. Obviously this cannot be done since the temperature sensitive quartz blank would not survive such a cycle.

The sealing equipment used optimized the adverse circumstances encountered in the sealing system. Good seal geometry (lack of re-entrancies and smooth fillets) is possible, and good quartz units can be sealed in glass holders.

5.3. Now that basic sealing principles have been discussed, fundamental methods for sealing the three glass holders will be described. The HC-(XM-2)/U and HC-(XM-3)/U holders are sealed using an induction heating technique. The HC-(XM-4)/U holder is sealed using a flame heating method.

The HC-(XM-2)/U and HC-(XM-3)/U holders are located and held in fixtures designed to push or squeeze the bulb and base together by a spring action. The holder is evacuated by placing this fixture under a bell jar during preheating and sealing. Heat is applied to the sealing area of the bulb and base through a Kovar ring which is an integral part of the base. This Kovar ring is heated by induction from an RF oscillator.

The bulb of the HC-(XM-4)/U holder is designed to be evacuated through the cylindrical open end of the bulb. Heat is applied to the seal area by a closely controlled flame. Working of the seal is accomplished only by a "push" from the differential in room air pressure and the evacuated enclosure itself. After the actual glass-to-glass seal has been completed and flame annealed, the cullet end of the bulb is removed by sawing with an abrasive saw.

- 5.4. As described in Paragraph 4.1.6., sealing of pre-production samples was done in equipment developed by Philips

 Electronics Industries, Limited, and owned by the United States Government. For the benefit of those who may not be familiar with the work previously done by Philips

 Electronics Industries, Limited, permission has been obtained to reproduce portions of their report here.

 The publication to be quoted in this section is entitled, "RG-1, Glass Evacuated Crystal Holder Sealing Information And Equipment", published by Canadian Radio Manufacturing Corporation, Limited, Toronto, Ontario, CANADA (now known as Philips Electronics Industries, Limited). This booklet describes a holder similar to the HC-(XM-2)/U.
 - 5.4.1. The balance of Section 5.4. including figures, is extracted from the Philips work. Editorial modifications were made for reader clarity.

5.4.2. <u>Processing Principles</u>

5.4.2.1. <u>General Requirements Of Glass Holder</u>

<u>Crystal Sealer</u>

The requirements of the sealing device include:

a. Sealing must be carried out in vacuum or inert gas to eliminate the need of a tip-off.

5.4. (Continued)

5.4.2. <u>Processing Principles</u> (Continued)

5.4.2.1. General Requirements Of Glass Holder Crystal Sealer (Continued)

- b. Temperature of quartz crystal must
 be kept below 200 degrees Centigrade.
- c. Sealing program must be carefully controlled so that the preheat, sealing and annealing schedule can be reproduced.
- d. Proper alignment of bulb and base must be guaranteed.
- Controlled pressure must be applied between bulb and base during sealing.
- f. Outside dimensions must be kept within the specified tolerances during sealing.
- g. Vacuum pumps must have sufficient capacity to ensure satisfactory ultimate vacuum.
- Facilities must be provided to bake out the units during evacuation at a temperature of 150 degrees
 Centigrade.

5.4. (Continued)

5.4.2. <u>Processing Principles</u> (Continued)

5.4.2.1. General Requirements Of Glass Holder Crystal Sealer (Continued)

- i. The equipment must be such that it can be operated by an inexperienced operator.
- j. The production rate must be as high as possible consistent with the quality of the seal.

5.4.2.2. Mechanics Of The Sealing Operation

An RF sealing method is employed in which the seal between bulb and base is made by heating a glazed metal ring which fits between the two. In this way, it is possible to seal the bulb and base under vacuum and still maintain the plated quartz blank at a low temperature. The sealing operation is carried out on the machine outlined in Figures 3 and 4. The twelve sealing heads are indicated together with the load, evacuation, oven and sealing positions, Descriptions and drawings of

5.4. (Continued)

5.4.2. Processing Principles (Continued)

5.4.2.2. <u>Mechanics Of The Sealing Operation</u>
(Continued)

the sealing head, vacuum equipment heating fixture and heat programming device are given in the following sections.

5.4.2.3. Operation Of The Sealing Head

The operation of the sealing head

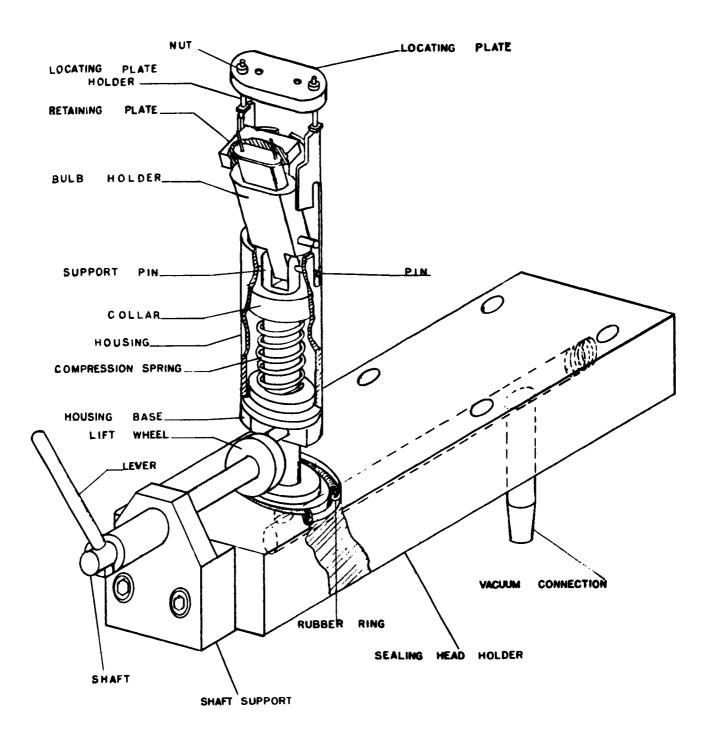
assembly is shown in Figures 5 and 6.

The sealing head assemblies are attached rigidly to the rotating table. Vacuum connection to each is made as described in Section 5.4.3.3. The sealing head assembly is constructed so that by turning the ejector lever, the bulb holder lowers and tilts forward into the loading position. While in this position, the bulb is placed in the bulb holder and the base with the sealed-on glazed metal ring is placed on the bulb. A ceramic retaining plate is placed over



44 - FIG.4

OPERATION OF SEALING HEAD



F19.5

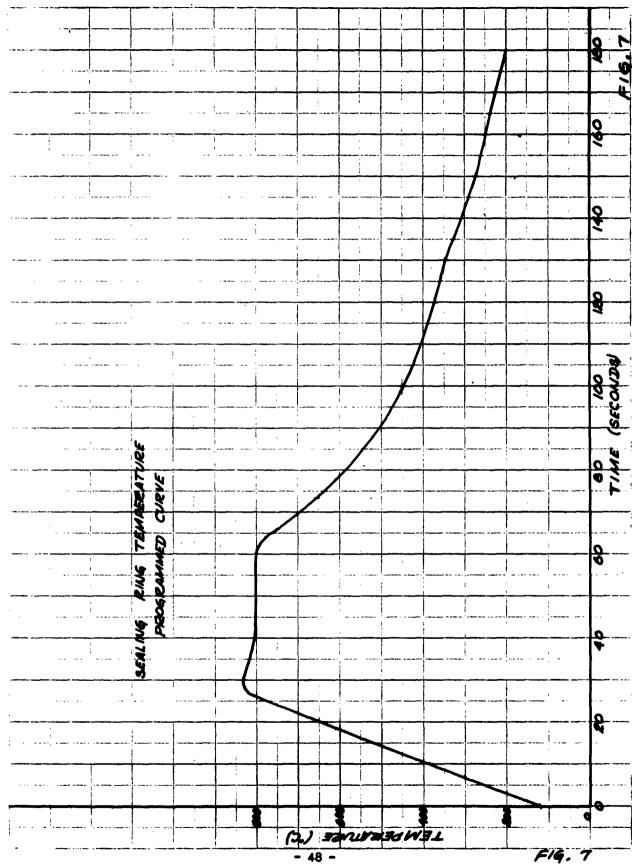


5.4. (Continued)

5.4.2. <u>Processing Principles</u> (Continued)

5.4.2.3. Operation Of The Sealing Head (Continued)
the base to ensure that the dimensions
of the sealed unit satisfy the specified
dimensions. When the ejector lever is
turned back, the loaded bulb holder
returns to a vertical position, rises
and presses against the ceramic
locating plate, under spring pressure.
The position of the bulb holder and
the locating plate guarantee the
alignment of the bulb and base.

When the bulb holder is in the sealing position and the ejector lever is retracted, a bell jar is placed over the sealing head assembly. The ground surface of the bell jar seals on a rubber 0-ring fitted in the base plate. The top of the bell jar is shaped so that the concentrator in the RF coil can be placed as close as possible to the metal sealing ring.



5.4. (Continued)

5.4.2. <u>Processing Principles</u> (Continued)

5.4.2.4. Sealing Cycle

The sealing cycle must be carefully controlled to obtain a satisfactory preheat, sealing and annealing schedule. A typical variation of temperatures of the metal sealing ring during the sealing operation is shown in Figure 7. The temperature increases slowly to a maximum temperature of 840 degrees Centigrade, decreases slowly due to conduction cooling during sealing, and them decreases gradually to a temperature of approximately 200 degrees Centigrade. This temperature cycle is completed in a period of three minutes. The unit is allowed to cool in vacuum for a period of three minutes and in air for a period of six minutes before it is removed from the sealing assembly.

5.4.2.5. Pre-Sealing Treatment Of Holder Parts

As the HC-(XM-2)/U holder parts are made of glass, cleaning problems are reduced.

The inside of the bulb is brushed free of dirt with a nylon brush and then scrubbed

5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)

machine.

5.4.3.1. Sealing Machine (Continued) twelve sealing heads and one induction heating coil are used. One crystal unit can be sealed for each index of the

The time in the rest position can be varied up to a period of ten minutes. However, three minutes has been determined as the minimum time required to obtain a satisfactory seal. During this time the preheat sealing and annealing occur. The time required between rest positions is fifteen seconds. Hence, the machine equipped with twelve sealing heads gives an output of eighteen sealed units per hour.

To increase production, more sealing heads up to a maximum total of four can be added to each rest position.

The vacuum connections are described in Section 5.4.3.3. A bake out oven is mounted over Pumping Positions 2 to 8.

5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.4.3.1. Sealing Machine (Continued)

In this way the units can be baked out at a temperature of 150 degrees

Centigrade during evacuation.

5.4.3.2. Sealing Heads

The operation of the sealing head has been described in Section 5.4.2.3.

The assembly drawing and various details are given in the drawings found in Appendix under SK-I-59-D-I through SK-I-59-D-28 inclusive.

5.4.3.3. <u>Vacuum Equipment</u>

Satisfactory evacuation is achieved by means of four Welch Duo-Seal two-stage high vacuum pumps, Model No. 1405. Each sealing position is connected to the center rotating vacuum valve through a shut-off valve and glass oil trap. The shut-off valve can be used to isolate each head from the vacuum system in case of emergency. The pumps are connected as shown in Figure 3.

5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.4.3.3. <u>Vacuum Equipment</u> (Continued)

The units are rough pumped in Positions 2 and 3 (Vacuum Pump I). The second pump is used on Positions 4, 5 and 6. The third pump operates on Positions 7 and 8. The fourth vacuum pump is used on the sealing position, Position 9, in order to obtain a high pumping speed during the sealing operation.

The center rotating valve is plugged in Position 10 so that the bell jar remains under vacuum although not connected to a vacuum pump. This aids in annealing the unit as it cools while under vacuum. In Positions II and I2 the bell jar is opened to the atmosphere so the unit is cool enough to handle in Position I.

The vacuum in the bell jar measured in the various rest positions by means of a McLeod gauge gave the following results:

5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.4.3.3. <u>Vacuum Equipment</u> (Continued)

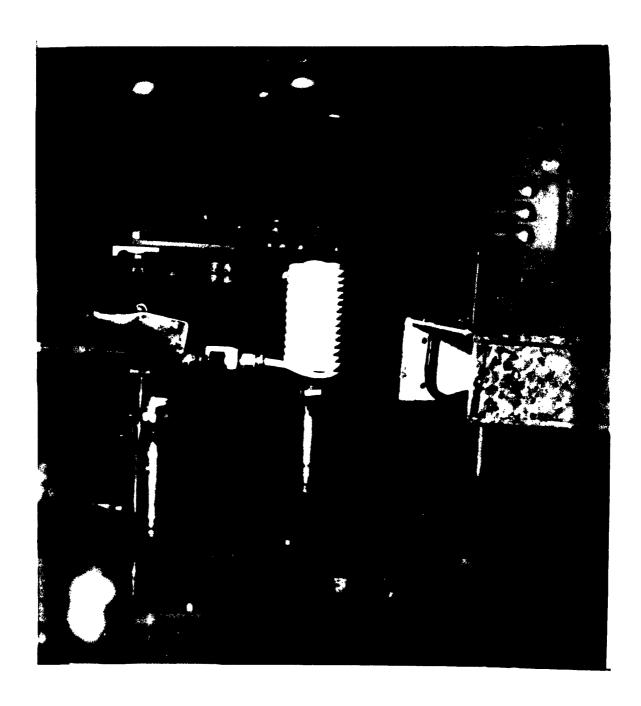
Position	Pressure (Microns Of Ha)
2, 3	75
4, 5, 6	30
7, 8	25
9 during sealin	g 75

5.4.3.4. <u>Heating Fixture</u>

The RF coil is formed from copper tubing covered with glass insulation.

Water is supplied to the coil by means of flexible rubber tubing. The rate of flow is maintained at approximately 0.3 gallons per minute. See Figure 8.

A concentrator in the form of a split copper cylinder with an end plate fits inside the coil. The end plate has an opening which fits the outside top dimension of the bell jar. This concentrates the heat in the area of the metal sealing ring. The concentrator has been rigidly mounted since its position is critical. The concentrator is air cooled to prevent changes in its characteristics with heat.



- 55 -

FIG.8

5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.4.3.4. <u>Heating Fixture</u> (Continued)

The RF oscillator employed to supply power to the induction heating coil in the present setup is a Philips Type No. E.4 385 09 rated at 8 KW, 200 amps. and designed to operate on 380 volts, 50 cycles. Since the output of this apparatus is much more than is required, it has been modified to operate on 220 yolt, 3 phase. 60 cycle. A sensing coil consisting of three turns of copper rod is mounted rigidly above the work coil support.

The coil assembly is raised and lowered by means of a cam on the main drive shaft of the machine.

5.4.3.5. Heat Programming Device

The induction heating required for the sealing operation must be regulated and programmed. To accomplish both these operations a servo-loop is employed together with a cam driven reference

5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.4.3.5. Heat Programming Device (Continued)
voltage. A block diagram of this
equipment is shown in Figure 9. The
function of the various units is
described below.

a. Work Coil

The induction heater work coil surrounds a specially designed concentrator as described in Section
5.4.3.4. The concentrator localizes
the heat in the area of the metal
sealing ring.

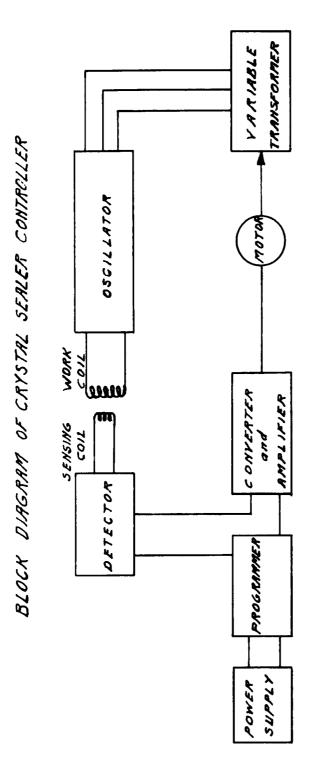
b. <u>Sensing Coil</u>

Immediately above the work coil is the sensing coil. The pick up on this coil is proportional to the field in the work coil.

c. <u>Detector</u>

Mounted immediately behind the work and sensing coils and connected to them by flexible leads is a box containing the detector circuit.

This consists of a selenium



CONTROL

5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued) 5.4.3.5. <u>Heat Programming Device</u> (Continued)

c. <u>Detector</u> (Continued)

rectifier and associated filter

circuitry for converting a portion

of the R F. signal to a D.C. value.

The output signal is built up

across the IO ohm resistor in

Figure IO.

d. <u>Programmer</u>

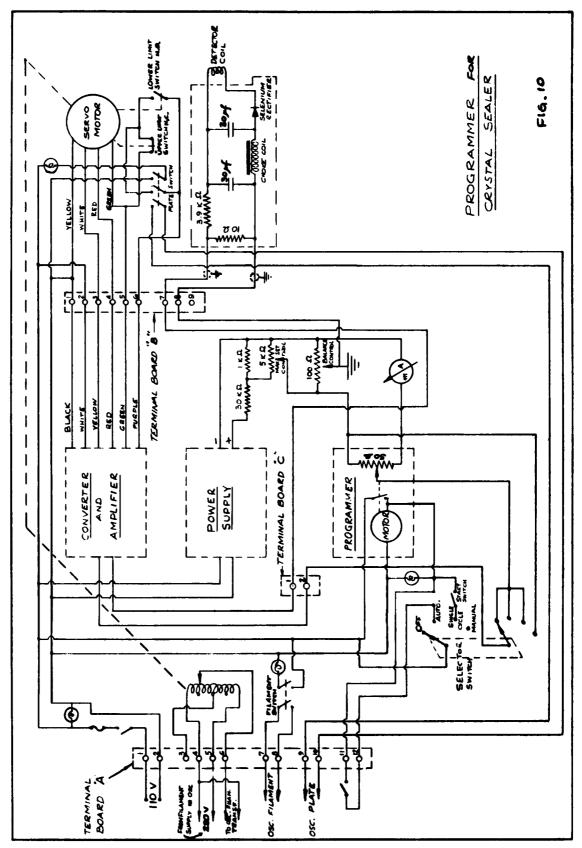
The three-minute work cycle is programmed by a synchronous motor driving a specially designed cam.

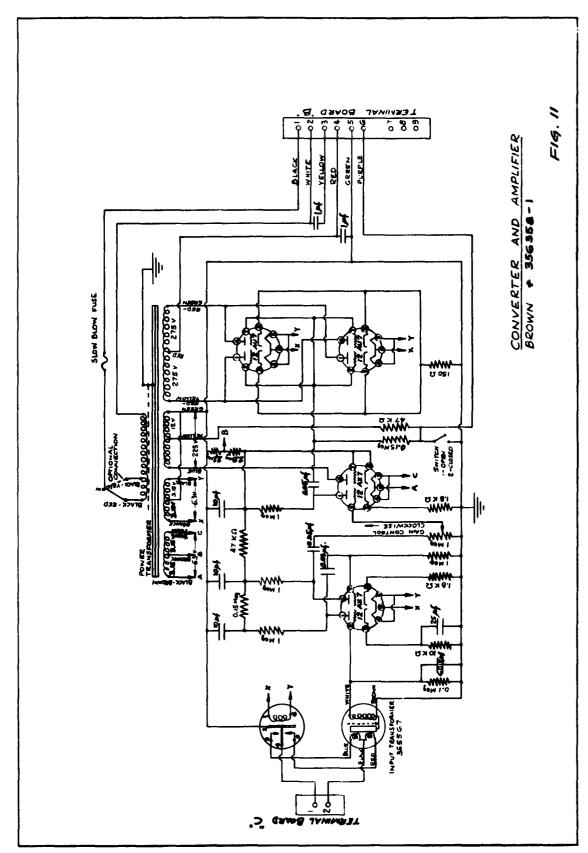
By means of a rocker arm system the radial variations of the cam are transmitted as angular motion to a potentiometer. A programmed reference voltage is thus obtained from the slides of the potentiometer. A limit switch is provided to synchronize this cycle with that of the rotating table.

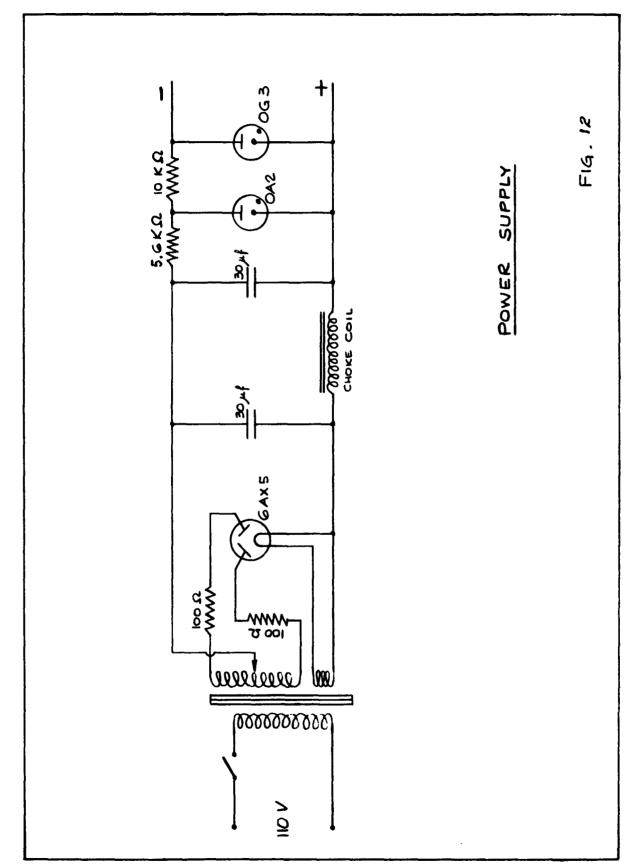
- 5.4. (Continued)
 - 5.4.3.5. <u>Heat Programming Device</u> (Continued)
 - e. Reference Voltage Power Supply

 To maintain the reference voltage independent of supply variations, a regulated power supply is provided. This consists of a normal rectifier circuit followed by an OA2 voltage regulator. To assure the utmost in stability this is followed by an OG3 voltage reference tube.
 - f. Converter And Amplifier

 The difference in voltage between the programmer output and the detector output is fed to the Brown converter and amplifer unit, No. 356358-1. This unit converts the difference or error signal to 60 cycle A C. and amplifies it sufficiently to drive the servo motor. The phase of the output relative to the 60 cycle line depends on the polarity of the







- 5.4. (Continued)
 - 5.4.3. Sealing Machine Descriptive Information (Continued)

 5.4.3.5. Heat Programming Device (Continued)
 - f. Converter And Amplifier (Continued)
 error signal and the direction
 of the servo motor rotation
 depends on this phase. The gain
 of this amplifier is adjustable
 by means of a slotted shaft recessed
 in the top of this chassis.
 - g. Servo Motor And Power Controller
 The servo motor is geared to a
 variable transformer. This
 transformer has a maximum rating
 of 9 amps at 220 volts. This
 system has been designed to
 control the induction heating
 unit by varying the filament
 voltage of the oscillator tube.
 The gear train between the motor
 and variable transformer has
 been designed to minimize
 overshoot due to the thermal lag
 inherent in such a control
 system. If plate supply control

5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.4.3.5. <u>Heat Programming Device</u> (Continued)

(Continued)
is provided for in the induction
heater, then the servo motor may
be geared to this control. In
this case, the response time will
be limited by the torque available
from the servo motor. The motor
is rated at 30 inch ounces and
20 R.P.M.

g. Servo Motor And Power Controller

h. Induction Heating Oscillator

The oscillator employed in the present set-up is described in Section 5.4.3.4.

i. Control Panel

The circuit diagrams for the control system are shown in Figures 10, 11 and 12. Filament switch, plate supply switch and indicator lights are provided for the oscillator. The control system is designed to obtain its

- 5.4. (Continued)
 - 5.4.3. Sealing Machine Descriptive Information (Continued)

 5.4.3.5. Heat Programming Device (Continued)
 - i. Control Panel (Continued)

 power from the oscillator to

 insure interlocking of the control

 system. As a safety feature, the

 variable transformer runs to zero

 when the plate supply is turned

 off. A selector switch determines

 the mode of operation. In the

 automatic position, the programmer

 is started by the rotation of the

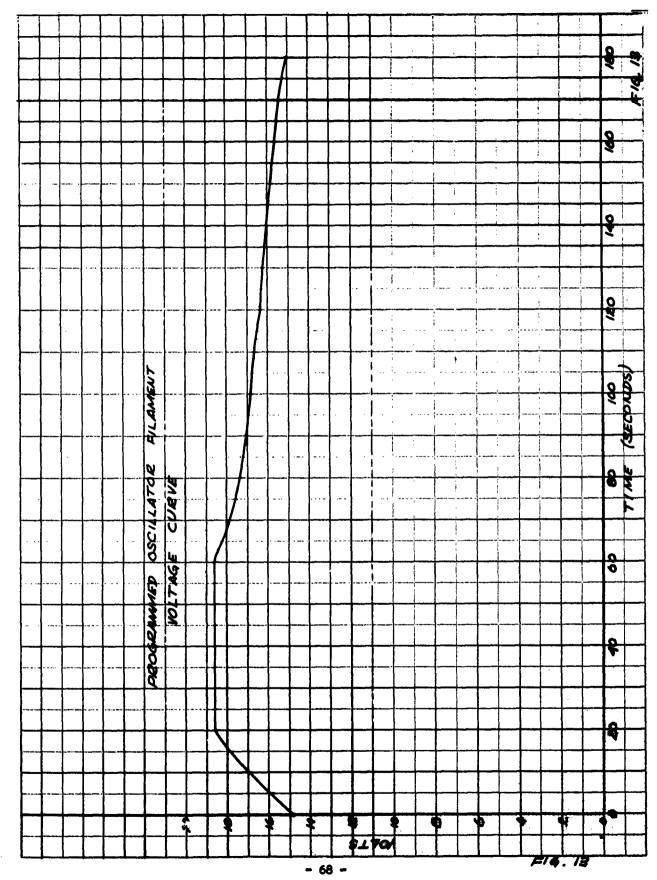
 sealing table.

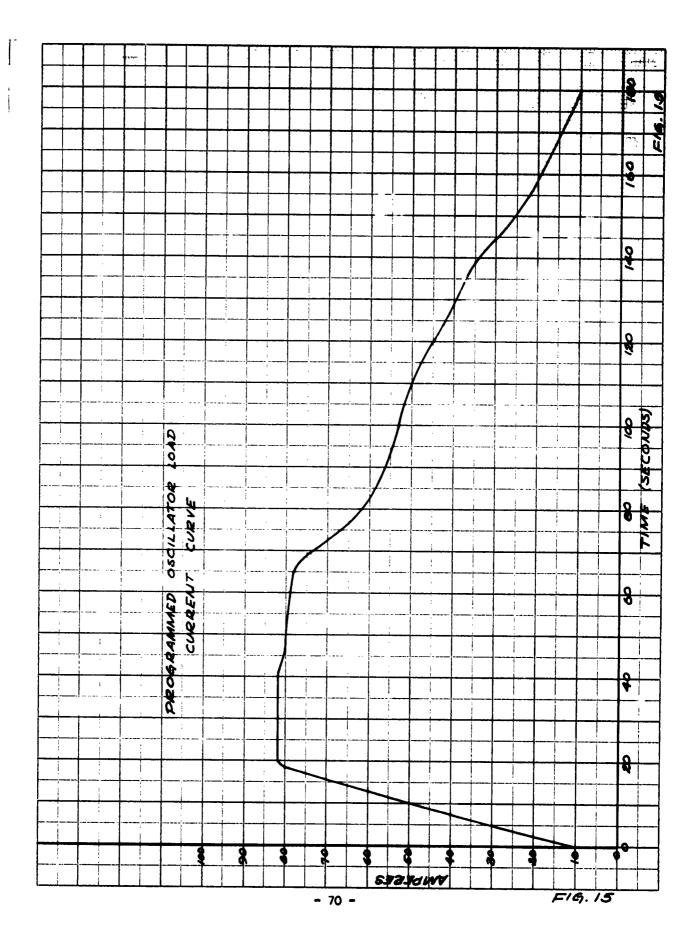
In the single cycle position, momentarily pressing of the start button will program a single cycle. In the manual position the oscillator power may be controlled by the panel control. A meter is provided for accurate indication of the reference setting. In the automatic position, the meter indicates the

- 5.4. (Continued)
 - 5.4.3. Sealing Machine Descriptive Information (Continued)
 5.4.3.5. Heat Programming Device (Continued)
 - ii. Control Panel (Continued)

 maximum reference setting. In the manual position, the meter indicates the actual reference setting. A screw adjustment is provided for balancing the system at the minimum power end. Operation of the programmer is indicated by a separate panel light. The panel control adjusts the maximum reference voltage in the automatic and single cycle positions and the actual reference voltage in the manual position.

Typical programmed oscillator characteristics are shown in Figures 13, 14, and 15. These include filament voltage, plate current and load current variations for the three minute sealing period.





5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued) 5.4.3.6. <u>Installation</u>

5.4.3.6.1. Sealing Machine

The required services for the sealing machine are:

- a. Electrical supplies
 220 volt 3 phase
 60 cycle 30 amps
 110 volt
 60 cycle 25 amps
- b. Water feed 20 gallonsper hour
- c. An inductive heating
 unit of approximately
 5 KW rating is required
 with suitable electrical
 and water supplies.

5.4.3.6.2. R.F. Oscillator

The control system for the crystal sealer is designed for an induction heater which employs 220 volts, 60 cycle in its control system. If higher voltages

5.4. (Continued)

5.4.3.6. <u>Installation</u> (Continued)

5.4.3.6.2. R.F. Oscillator (Continued)

are employed, then two
additional relays and two
auto transformers will be
required.

Install the oscillator unit as close to the sealer as possible. Connect control lines to oscillator as indicated in Figure 10. Terminal Strip A may be reached by opening the control box beneath the sealer. Connect R.F. lines to output of oscillator. If possible, obtain water supply for work coil through oscillator water pressure interlock. Adjust flow rate to 0.3 gallons per minute.

5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.4.3.7. <u>Setting-Up Instructions</u>

5.4.3.7.1. Single Cycle Operation

- a. Rotate sealer table and stop with work coil between heads.
- b. Pull out control chassis
 and remove cover.
- c. Replace control chassis without cover in such a manner that rotation of variable transformer may be observed.
- d. Turn on water for oscillator and load coil.
- e. Set selector switch to
 manual and if programmer
 light comes on, wait
 until it extinguishes.
- f. Set setting control to minimum.
- g. Turn on programmer switch and oscillator heater switch. (Plate switch off.)

- 5.4. (Continued)
 - 5.4.3. Sealing Machine Descriptive Information (Continued)

5.4.3.7. <u>Setting-Up Instructions</u> (Continued)

5.4.3.7.1. Single Cycle Operation
(Continued)

- h. After short warm-up,
 variable transformer
 should turn to low end
 and oscillate slowly.
 If balance control is
 out of adjustment,
 there will be no
 oscillation.
- i. Adjust balance control for point where oscillation is just noticeable.
- j. Turn on plate switch and adjust balance control so that variable transformer moves very slowly, clockwise. This must be done before oscillator starts to indicate load current. If adjustment is not completed before

- 5.4. (Continued)
 - 5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)
 - 5.4.3.7. <u>Setting-Up Instructions</u> (Continued)
 - 5.4.3.7.1. <u>Single Cycle Operation</u>

(Continued)

- j. (Continued) this occurs, turn off plate switch. As soon as variable transformer has turned to low end, repeat Step j.
- k. When Step j. has been completed, the variable transformer should rotate clockwise and finally stop at the point where load current is just apparent.
- Slowly increase the setting control. The oscillator output will follow. Set at 50 amps load current.

- 5.4. (Continued)
 - 5.4.3. Sealing Machine Descriptive Information (Continued)
 5.4.3.7. Setting-Up Instructions (Continued)
 - 5.4.3.7.1. Single Cycle Operation
 (Continued)
 - m. Adjust the amplifier gain control (inside control box on top of amplifier) to just below the point at which rapid heating occurs. Return setting control to zero.
 - n. Start pumps and obtain a vacuum in sealing position better than 25 microns of mercury.
 - Load unit with bases and bulbs and rotate into sealing position.
 - p. Slowly advance setting control until temperature is 810 degrees Centigrade.
 Do not leave setting control in this high position for longer

- 5.4. (Continued)
 - 5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)
 - 5.4.3.7. <u>Setting-Up Instructions</u> (Continued)
 - 5.4.3.7.1. Single Cycle Operation
 (Continued)
 - p. (Continued) than thirty seconds. Repeat at one minute intervals if necessary to get setting for correct temperature.
 - q. Turn selector switch to single cycle and set setting control for the 810 degrees Centigrade maximum setting obtained in Step p.
 - r. Rotate a new unit into position and turn off table control.
 - s. Press start button and hold until programmer light remains lit when recleared. Oscillator should program as indicated in Figure 14.

- 5.4. (Continued)
 - 5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)
 - 5.4.3.7. <u>Setting-Up Instructions</u> (Continued)
 - 5.4.3.7.1. Single Cycle Operation
 (Continued)
 - t. After approximately three minutes, programmer light will go out and table may be rotated.
 - u. Leave head containing sealed unit in cooling position under vacuum for at least three minutes, before rotating to loading position.
 - v. Replace cover on control box and place unit in proper position. Once satisfactory seals have been obtained in the single cycle position, automatic operation may be initiated.

5.4. (Continued)

5.4.3.8. Operating Instructions (Continued)

5.4.3.8.1. Sealing Machine

- a. Turn selector switch to "Off".
- b. Turn on controller and set setting control to value obtained in Step p.
- c. Start vacuum pump oven and oscillator filament.
- d. Set table timer for 3.05 minutes or more and start.
- e. Load crystal units as table passes loading position.
- f. When first crystal unit rotates into the position immediately before the sealing position, turn selector switch to automatic and turn on plate voltage.

5.4. (Continued)

5.4.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.4.3.8. <u>Operating Instructions</u> (Continued)

f. (Continued)

5.4.3.8.1. <u>Sealing Machine</u> (Continued)

Be sure table has stopped before turning switches.

It is important that the programmer does not operate on empty heads.

g. While the last crystal is being sealed, turn selector switch to "Off".

5.4.3.8.2. Crystal Loading

- a. Remove glass bell jar.
- Open sealing head to loading position, turning handle counterclockwise.
- c. Place bulb in bulb holder.
- d. Place base assembly onto bulb.
- e. Place ceramic retaining plate over base.

- 5.4. (Continued)
 - 5.4.3.8. <u>Operating Instructions</u> (Continued)

5.4.3.8.2. Crystal Loading (Continued)

- f. Raise sealing head into sealing position by turning handle clockwise.
- g. Place bell jar over sealing head.
- 5.4.4. Sealing Process Fault Location And Correction

 A table of the more common faults which may occur
 in sealed crystal units are listed below together
 with their causes. Included also are the adjustments which should be made to the sealing machine
 when these faults occur in excessive proportions.

5.4.4.1. <u>Crystal Characteristics</u>

a. Fault: Frequency increases

Cause: Overheating

Correction: Reduce power input to

heating fixture.

- 5.4. (Continued)
 - 5.4.4. <u>Sealing Process Fault Location And Correction</u>
 (Continued)
 - 5.4.4.1. Crystal Characteristics (Continued)
 - b. Fault: Frequency decreasesCause: Contamination from handling

or sealing machine

Correction: Improve cleanliness

the following: sealing

of one or more of

jig, bell jar, holder

parts.

Cause: Decomposition of cement

Correction: Reduce amount of

cement and ensure

proper curing.

c. Fault: Quartz develops high resistance or refuses to oscillate. (Silver base coat may have become

coal may have become

yellowish or translucent.)

Cause: Severe overheating

Correction: Reduce power to heating

fixture.

5.4. (Continued)

5.4.4. <u>Sealing Process Fault Location And Correction</u> (Continued)

5.4.4.1. <u>Crystal Characteristics</u> (Continued)

c. (Continued)

Cause: Blank mounted too low in holder. Blank mounted too high in holder resulting in clamping.

Correction: Raise blank to

position at least
.050 inches above

5.4.4.2. Glass Defects

a. Fault: Cracks starting from the

base seal during sealing

or later during tempera
ture cycling, or leaky

base seal

Cause: Underheating

Correction: Increase power to heating fixture,

5.4. (Continued)

5.4.4. <u>Sealing Process Fault Location And Correction</u> (Continued)

5.4.4.2. Glass Defects (Continued)

b. Fault: Poor vacuum

Cause: Defective holder parts

Cause: Excessive cement used

Correction: Reduce amount of

cement and ensure

proper curing.

Cause: Poor sealing machine

vacuum

Correction: Repair vacuum system.

5.5. The same sealing techniques as described in Paragraph 5.4.

above were used for sealing the HC-(XM-3)/U holder.

There is no need to be redundant.

- 5.6. As described in Paragraphs 4.1.6. and 5.4., sealing of pre-production samples was done on equipment developed by Philips Electronics Industries, Limited, and owned by the United States Government. Again, for the benefit of those who may not be familiar with the work previously done by Philips Electronics Industries, Limited, permission has been obtained to reproduce portions of their reports here. The publication to be quoted in this section is entitled. "RG-2, Glass Evacuated Crystal Holder Sealing Information And Equipment", published by Canadian Radio Manufacturing Corporation, Limited, Toronto, Ontario, CANADA, now known as Philips Electronics Industries, Limited. This booklet describes a holder similar to the HC-(XM-4)/U.
 - 5.6.1. The balance of Section 5.6., including the figures, is extracted from the Philips' work.

 Editorial modifications were made for reader clarity.

5.6.2. <u>Processing Principles</u>

5.6.2.1. General Requirements Of A Glass Crystal
Holder Sealing Machine

The requirements of the sealing device include:

a. Sealing and pumping must be done simultaneously to eliminate the need of a tip-off.

5.6. (Continued)

5.6.2. <u>Processing Principles</u> (Continued)

- 5.6.2.1. <u>General Requirements Of A Glass Crystal</u>

 <u>Holder Sealing Machine</u> (Continued)
 - Temperature of quartz crystal must
 be kept below 200 degrees Centigrade.
 - c. Proper alignment of bulb and base must be ensured during sealing.
 - d. Method should result in reproducible seals.
 - Vacuum pump must have sufficient capacity to ensure satisfactory exhaust.
 - f. The equipment should be such that it can be operated by a semi-skilled worker.
 - g. The production rate must be as high as possible consistent with the quality of the seal.
- 5.6.2.2. Mechanics Of The Sealing Operation

 A flame sealing method is employed in which the seal is made while the unit is being evacuated through an extension of the bulb. In this way it is possible to seal the bulb and base

5.6. (Continued)

5.6.2. <u>Processing Principles</u> (Continued)

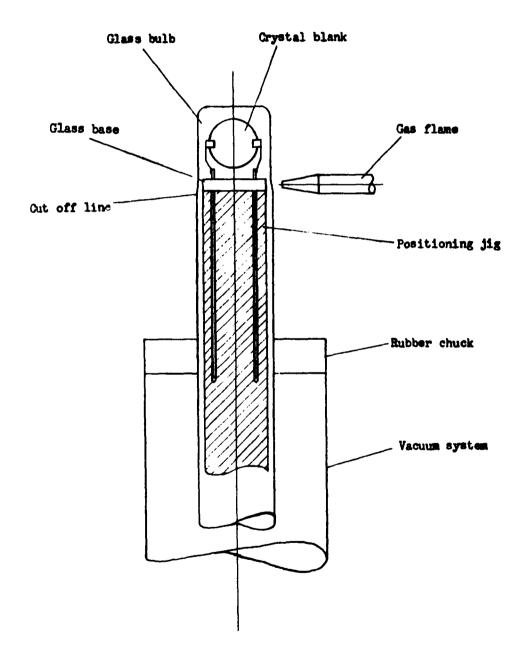
5.6.2.2. <u>Mechanics Of The Sealing Operation</u> (Continued)

leaving a vacuum in the unit and still maintain the plated quartz blank at a sufficiently low temperature. The arrangement which is used to carry out this method of sealing is shown in Figure 16.

The crystal blank is mounted on a glass base, the leads of which are inserted in a positioning jig. This accurately fixes the position of the base. The glass bulb, which in the area of the seal closely fits the shape of the base, is placed over the base assembly.

A vacuum tight connection is made to the vacuum system by means of the chuck.

After the unit has been pumped for some time and while it is still being evacuated, the bulb and base are sealed



- 5.6. (Continued)
 - 5.6.2. Processing Principles (Continued)
 - 5.6.2.2. Mechanics Of The Sealing Operation
 (Continued)

together by means of a gas flame. A very fine flame is employed which rotates around the seal area at a very slow rate. The flame support is pivoted so that the position of the flame relative to the seal can be controlled by means of a cam. The difference in pressure between the outside and inside of the bulb (I atmosphere) causes the builb to collapse onto the base at a temperature considerably lower than that required if no pressure difference existed. In this way a small length of seal is made at one time while the rest of the seal area is cool. With this method the crystal remains at a sufficiently low temperature and the relative position of the bulb and base is maintained.

- 5.6. (Continued)
 - 5.6.2. Processing Principles (Continued)
 - 5.6.2.2. Mechanics Of The Sealing Operation
 (Continued)

After the seal has been completed, the unit is removed from the rubber chuck and the glass tubulation is removed.

This leaves the evacuated glass enclosed crystal unit of dimensions which can be reproduced to close tolerances.

As the HC-(XM-4)/U holder parts are made of glass, cleaning problems are reduced. The inside of the bulb is brushed free of dirt with a nylon brush and then scrubbed with pure alcohol and washed in three changes of boiling distilled water. The bases are cleaned in the same manner. The parts are dried in a vacuum oven at 150 degrees Centigrade for several hours.

5.6. (Continued)

5.6.2. <u>Processing Principles</u> (Continued)

5.6.2.3. <u>Pre-Sealing Treatment Of Holder Parts</u> (Continued)

Vacuum bakeout at even higher temperatures up to the softening point of glass is suggested for all holder parts in order to remove absorbed contamination and gases.

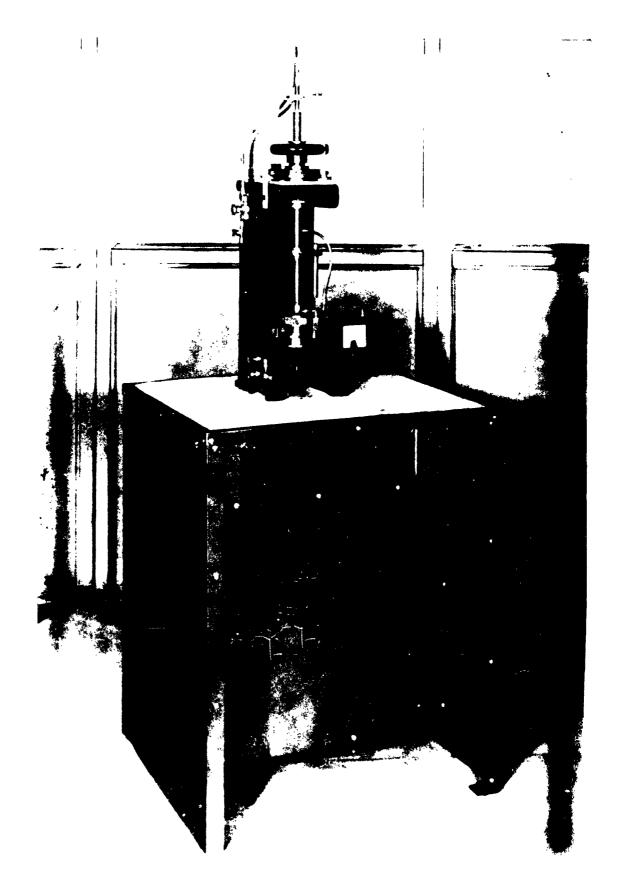
After cleaning, holder parts are stored in a dry, dust-free atmosphere.

5.6.3. <u>Sealing Machine Descriptive Information</u>

5.6.3.1. Sealing Machine

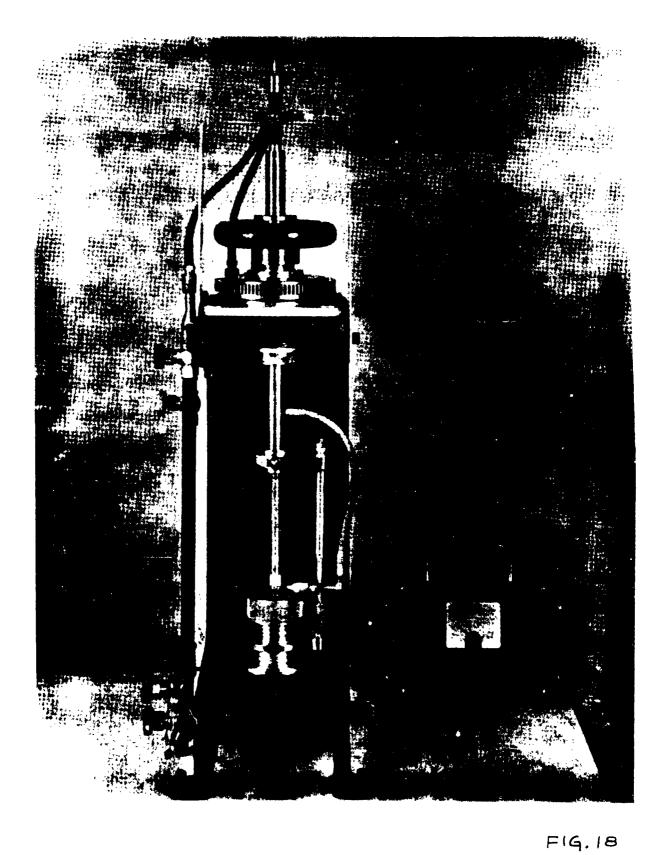
A single-head sealer has been designed and built, employing the sealing method described in Paragraph 5.6.2 2. and Figures 17 and 18. The construction of the sealer is shown in Figures 19, 20, 21, and 22.

A stationary chuck aligns the glass bulb and base in the correct position relative to height and concentricity. A small rotation of the compression cap enables the work to be clamped or



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F14.17



5.6. (Continued)

5.6.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.6.3.1. <u>Sealing Machine</u> (Continued)

Around the main body of the chuck is mounted a cam with a profile duplicating the outside shape of the glass bulb.

A rotating tube, in line with the axis of the chuck, supports a pivoted arm. A gas oxygen burner is mounted on the pivoted arm in such a way that it can be adjusted initially. As the tube rotates, the distance from the burner to the work is controlled by a cam follower, located at the bottom of the arm. This follower rides on the cam profile mounted on the chuck. The height of the flame is adjusted by means of the hand operated collet on the rotating tube. A fixed tube mounted inside the rotating tube holds a retaining cup for supporting the bulb during sealing. The inside of the cup is lined with asbestos which fits tightly on the bulb to minimize the heat transfer to the crystal. Air can be supplied to the cup to cool the bulb.

5.6. (Continued)

5.6.3. <u>Seating Machine Descriptive Information</u> (Continued)

5.6.3.1. <u>Sealing Machine</u> (Continued)

The premixed gas and oxygen is fed into the fixed tube through an opening into the rotating tube and through a flexible hose to the burner.

The upper head is driven through a gear train from a vertical shaft which is coupled to a gear reducer motor combination. The rate of rotation of the flame is approximately four revolutions per minute.

An auxiliary hand flame is used to preheat the seal area before sealing and to anneal the seal after sealing.

The electrical circuit diagram for the sealing machine is shown in Figure 23.

5.6.3.2. <u>Vacuum System</u>

Satisfactory evacuation is achieved by means of a Welch Duo Seal two-stage high vacuum pump (Model No. 1405). An electrically controlled valve is included in the vacuum line in order to isolate

5.6. (Continued)

5.6.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.6.3.2. <u>Vacuum System</u> (Continued) the pump during loading. A Pirani vacuum gauge is connected to the vacuum line, in order to measure

5.6.3.3. Installation

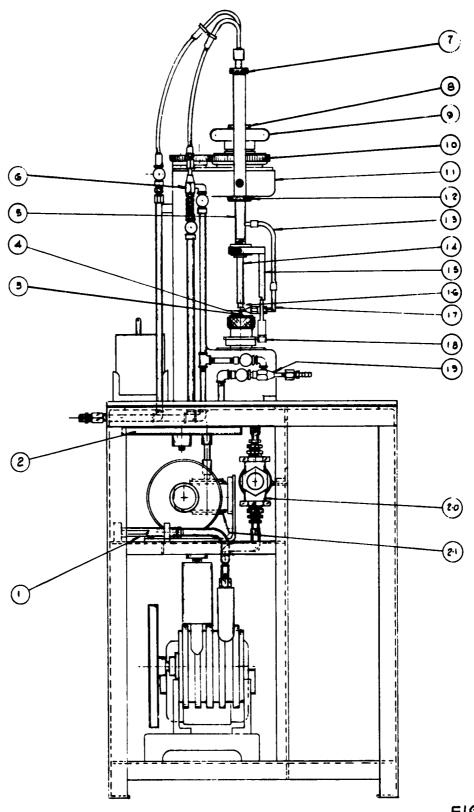
the vacuum.

The required services for the sealer are:

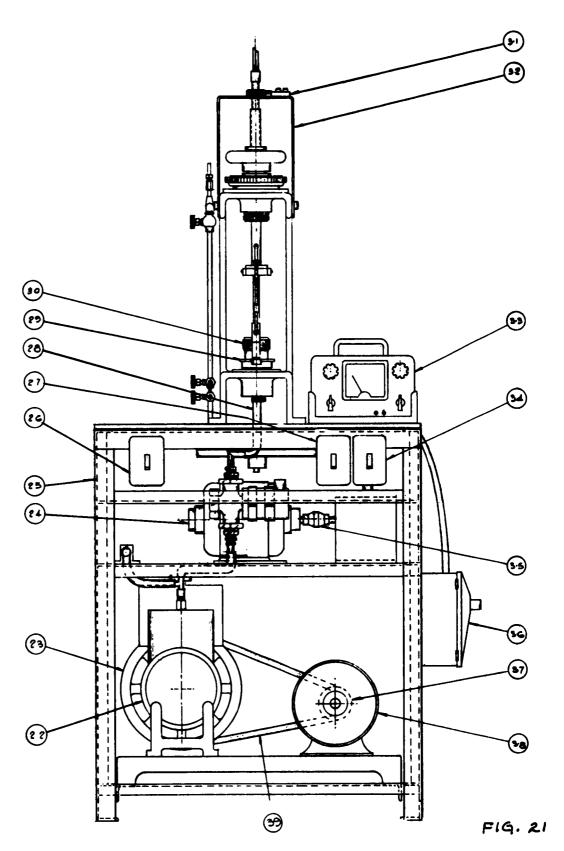
- a. Electrical supply 110 volt60 cycle 20 amperes
- b. Gas
- c. Oxygen
- d. Low pressure air

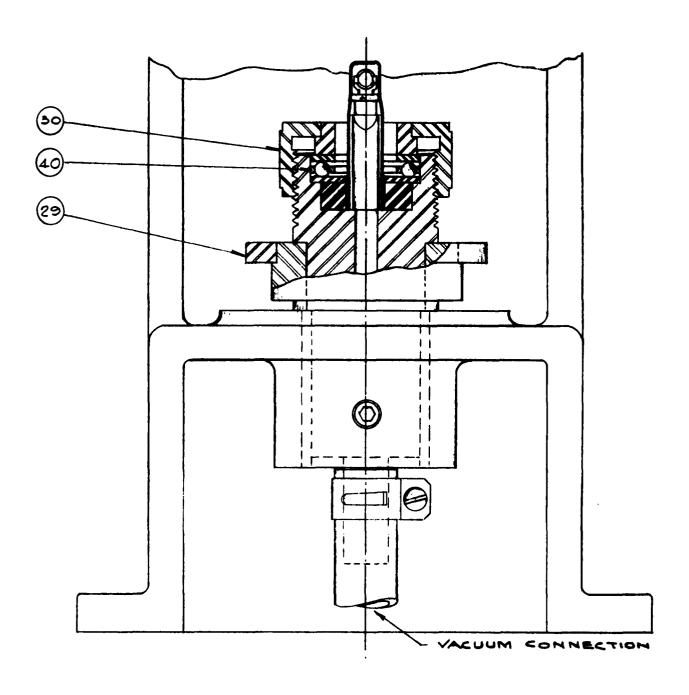
5.6.3.4. Setting-Up Instructions

- a. Connect services to sealer.
- b. Load base and builb, and checkthat the alignment is satisfactory.
- c. Lower stationary tube holding retaining cup and check alignment.
- G. Turn on vacuum pump and check that vacuum comes down to less than 100 microns Hg.



F19.20





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F19.22

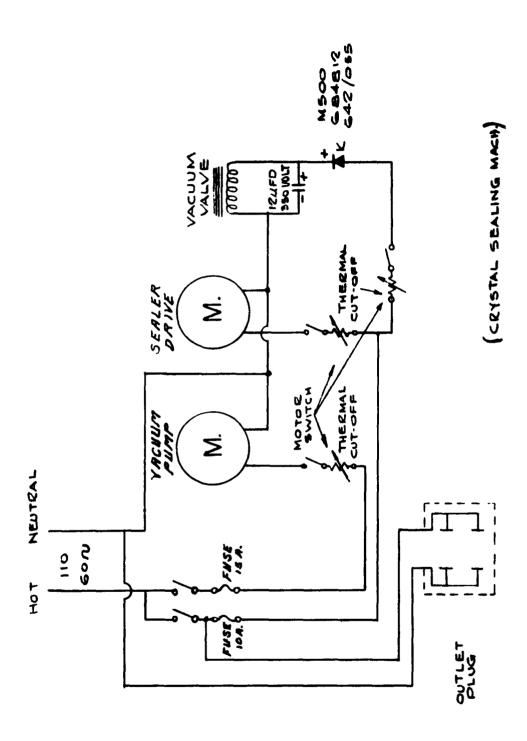


FIG. 23

5.6. (Continued)

5.6.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.6.3.4. <u>Setting-Up Instructions</u> (Continued)

- e. Light flame in rest position and swing burner to sealing position for base. Check that burner is directed to center point of support of burner. Adjust stop if necessary to bring height to center of base. Check that the distance from the burner to the bulb is satisfactory (approximately .150 inches).
- f. Start sealer motor. Adjust if necessary the flame to obtain a uniform seal. Seal should be complete in approximately one minute.

5.6.3.5. Operating Instructions

- a. Start vacuum pump with valve closed.
- b. Light flame in rest position, and turn on air for cooling.
- c. Load base on base support.
- d. Place bulb over base, insert as far as possible and clamp chuck by rotating compression cap.

5.6. (Continued)

5.6.3. <u>Sealing Machine Descriptive Information</u> (Continued)

5.6.3.5. Operating Instructions (Continued)

- e. Lower stationary tube to bring retaining cup over bulb.
- f. Open valve to vacuum system and evacuate to pressure of 100 microns
 Hg.
- g. Preheat the seal area with soft gas-air flame.
- h. Swing the flame to the sealing position and start sealer motor.
- After the seal has been completed, swing the sealing flame to rest position, and close vacuum valve.
 Open chuck by rotating compression cap.
- j. Anneal the seal area with a soft gas-air flame.
- k. Remove the sealed unit from the chuck.
- 1. Cut sealed unit to correct length.

5.6. (Continued)

5.6.4. Sealing Process Faults And Their Correction

The faults which occur in HC-(XM-4)/U crystal units which are related to the sealing process are usually the result of one of the following causes:

- a. Not sufficient heat used during sealing.
- b. Excessive heat at crystal element.
- c. Loading of the quartz.

Fault a., insufficient heat, results in poor vacuum, leaky seals, and glass cracks. It is corrected by increasing the flame heat and/or reducing the rate of rotation.

Fault b., excessive heat at the crystal element, results in an increase in frequency, an increase in resistance, and in the extreme case, failure to oscillate. This can be corrected by reducing the flame heat and/or increasing the rate of rotation. This fault also occurs if the quartz blank is mounted too close to the seal area.

Fault c., loading of the quartz element, results in a decrease in frequency which is caused by a transfer of contamination to the quartz element.

This can be corrected by improved cleaning of the holder parts or the sealing machine.

6. REVIEW BY HOLDER TYPE

6.1. <u>HC-(XM-2)/U Holder</u>

The initial design of this holder followed very closely that of the Philips RG-I holder. The only difference between the two designs is that the dimensional tolerances stipulated for the Corning holder are closer. So that the maximum amount of space is available within the bulb, the Corning nominal dimensions were slightly larger than those set by Philips. The initial designs for bulb and base major and minor diameters (the A, F, G, and J dimensions described in Section 4.2.) provided satisfactory results throughout the history of this project. The only changes required were those of bulb length and base thickness. The proper values for these dimensions were found by sealing experimentation.

Arrangements were made with L. L. Constantin And Company (succeeded by Isotronics, Inc.) of Lodi, New Jersey, to supply bases for the holders to Corning's specifications. Preliminary bulb and base samples were fabricated for sealing experimentation. Two special sealing beads were constructed to handle both the HO-(XM-2)/U and HC-(XM-3)/U holders. These sealing beads were for use on the Government owned sealing equipment located at Scientific Radio Products, Inc., Loveland, Colorado.

6. REVIEW BY HOLDER TYPE (Continued)

6.1. HC-(XM-2)/U Holder (Continued)

Section 4.1.6. of this report outlines the stipulation that the quartz blanks shall not exceed 250° C. during sealing. Initially it was intended to seal these holders without quartz blanks. Preliminary temperature indications were made using known melting point solders: 230° C., 250° C., and 285° C.

The expectations of this initial sealing work was to establish the final length dimension for the bulb and the optimum base thickness. The results were that good seals were achieved only when the 250° C. temperature was exceeded. Solders were attached to the middle of plated quartz blanks as well as to the spring mounting clips. These spring mounting clips cannot be made of the conventional spring steel wire, but must be fabricated from a suitable stainless steel alloy — such as Number 302. It is not the purpose of this project to perfect quartz mounting clips, so stainless steel wire was formed in the same manner as spring steel wire clips, and welded in place on the Kovar leads instead of soldered.

Based on the aforementioned sealing experience, contractual changes were made so that pre-production samples were submitted based not on meeting a 250° C. maximum quartz temperature limit, but on demonstrating

6. REVIEW BY HOLDER TYPE (Continued)

6.1. HC-(XM-2)/U Holder (Continued)

that good quartz crystals could be successfully sealed in the holders. In actuality, this modification is completely compatible with the intentions and desires of the Government and the crystal manufacturers.

A second sealing test with quartz blanks was conducted. This test was to determine the amount of "squeeze" of bulb and base encountered during the optimum sealing cycle. "Squeeze" is the difference in overall assembled base and bulb height before and after sealing. When a good seal with proper seal geometry has been made, the squeeze is .045".

Although supposedly good seals were made with quartz crystals, the environmental test phase of the pre-production sample lot was not successful. Poor seal geometry caused failures on thermal shock testing. As noted before, -55° C. to boiling water is a shock more severe than had previously been specified. Slight re-entrant angles in the seal area can be the source of seal failure when thermally shocked. These re-entrancies are avoided and minimized by devoting careful attention to alignment of bulb and base in the sealing fixture.

A third pre-production test was conducted with quartz crystals sealed. These units, sealed at Philips

6.1. HO-(XM-2)/U Holder (Continued)

Electronics Industries, Limited, met the environmental test requirements. Nineteen holders with quartz crystals of the following frequencies, 2.85, 40 and 70 Mc, were sealed as part of this pre-production test. Frequency and resistance before and after sealing are tabulated. No particular attempts were made to produce an exact frequency. The use of the quartz crystals demonstrated that good units can be sealed in glass holders.

Nominal Before Seal Seal (apm) Seal Seal Seal Seal Seal Seal Seal Seal			<u>C</u>	Free	quency on non		nail	Fr	equency		tance
Fraguency Seal Seal (apm) Seal Seal 2.85 Mc + 3	Nomi	nal									After
" + 26			_5								Seal
" + 26	2 25	Ma	_	3		_	10	_	4.6	40	**
" + 20		PPC				_					
" + 16 + 2 - 4.9 45 36 " - 3 - 3 0 70 73 " + 20 + 1 - 6.7 88 23 " + 15 - 2 - 6.0 50 39 40 Mc - 320 - 312 - 0.2 27 17 " + 250 - 180 - 10.7 27 18 " + 50 0 - 1.3 25 16 " +2810 +2600 - 5.3 27 18 " + 160 + 470 + 7.8 27 18 " 0 + 360 + 9.0 27 20			•				_				
" - 3 - 3 0 70 73 " + 20 + 1 - 6.7 88 23 " + 15 - 2 - 6.0 50 39 40 Mc - 20 - 312 - 0.2 27 17 " + 250 - 180 -10.7 27 18 " + 50 0 - 1.3 25 16 " +2810 +2600 - 5.3 27 18 " + 160 + 470 + 7.8 27 18 " 0 + 360 + 9.0 27 20 70 Mc + 230 -2300 -36.1 49 38			+	2		-	13	_	2.3	5 0	42
" + 20 + 1 - 6.7 88 23 " + 15 - 2 - 6.0 50 39 40 Mc - 20 - 312 - 0.2 27 17 " + 250 - 180 -10.7 27 18 " + 50 0 - 1.3 25 16 " +2810 +2600 - 5.3 27 18 " + 160 + 470 + 7.8 27 18 " 0 + 360 + 9.0 27 20 70 Mc + 230 -2300 -36.1 49 38	11		+	16		+	2	_	4.9	45	3 6
" + 20 + 1 - 6.7 88 23 " + 15 - 2 - 6.0 50 39 40 Mc - 20 - 312 - 0.2 27 17 " + 250 - 180 -10.7 27 18 " + 50 0 - 1.3 25 16 " +2810 +2600 - 5.3 27 18 " + 160 + 470 + 7.8 27 18 " 0 + 360 + 9.0 27 20 70 Mc + 230 -2300 -36.1 49 38	Ħ		_	3		_			0	70	73
" + 15 - 2 - 6.0 50 39 40 Mc - 320 - 312 - 0.2 27 17 " + 250 - 180 -10.7 27 18 " + 50 0 - 1.3 25 16 " +2810 +2600 - 5.3 27 18 " + 160 + 470 + 7.8 27 18 " 0 + 360 + 9.0 27 20 70 Mc + 230 -2300 -36.1 49 38	11		+			+		_	6.7	88	
" + 250	11		+			-	2	-	6.0		
" + 250	40	Mc	_	20د		_	312	_	0.2	27	17
" + 50 0 - 1.3 25 16 " +2810 +2600 - 5.3 27 18 " + 160 + 470 + 7.8 27 18 " 0 + 360 + 9.0 27 20 70 Mc + 230 -2300 -36.1 49 38		• • •									18
" + 160 + 470 + 7.8 27 18 " 0 + 360 + 9.0 27 20 70 Mc + 230 -2300 -36.1 49 38	11										
" + 160 + 470 + 7.8 27 18 " 0 + 360 + 9.0 27 20 70 Mc + 230 -2300 -36.1 49 38	11		+2	2810		+2	2600	_	5.3	27	18
" 0 + 360 + 9.0 27 20 70 Mc + 230 -2300 -36.1 49 38	11										• -
	II		•								
	70	Mc	+	230		-:	2300		36. i	49	38
		• • •	+	580		_	1900	-	35.5	48	48
" + 30 -1300 -19.0 63 56	11										
" - 190 -1970 -25.4 62 47	11		_	190		_	1970	-	25.4	62	47
" - 160 -2700 -35.3 48 40	H		_								• -
" - 580 - 1830 - 17.9 61 51	11		_								

6.1. HC-(XM-2)/U Holder (Continued)

Pilot production of bulbs and bases was begun.

During this pilot run of bases, Corning Glass Works introduced a new material -- CLEARFORM^(R) ware. This material provides a means of producing 7052 precision shaped parts. These preformed parts were advantageously used to produce the clear glass bases. Since a new processing technique was introduced, plus a new base supplier, Tronex of Millville, New Jersey, another set of pre-production test samples was required. Samples were sealed and subjected to environmental tests and passed.

The pilot run was completed using the bulbs as approved in the third and fourth pre-production test. The bases used were made using the CLEARFORM $^{(R)}$ glass parts.

6.2. HC-(XM-3)/U Holder

Although this holder was not one which had previously been developed, the initial design followed exactly that used for the HC-(XM-2)/U holder with the exception of the bulb length and the length of the Kovar leads. As previously mentioned, sealing heads were designed and constructed to accommodate both the HC-(XM-2)/U and HC-(XM-3)/U holders.

The work done on the HC-(XM-2)/U holder showed that a maximum quartz temperature limit of 250° C. was not readily attainable. Normally the type of quartz units mounted in the comparable metal holders (HC-13/U) are held in place with solders that melt at temperatures below 200° C.

Initial sealing trials using Corning bulbs and bases from L. L. Constantin were conducted at Scientific Radio Products, Inc. Like the HC-(XM-2)/U holder, the 250° C. limit was exceeded -- as measured with the known melting point solders.

Although all holders of this contract carried the 250° C. maximum quartz crystal temperature limit, only the HO-(XM-2)/U and HO-(XM-4)/U holders had been developed for actual quartz units. Since this is an Industrial

6.2. HO-(XM-3)/U Holder (Continued)

Preparedness Contract, development of a special quartz crystal mounting technique was beyond the original scope and intent. Nevertheless the approach was taken that possibly higher temperature solders and/or welding could be used for crystal mounting.

Previous sealing work with the HC-(XM-2)/U holder indicated that the temperature adjacent to the seal area at a point where the quartz units would be mounted would be at a temperature of 300° C. or more. Solders, metals, or alloys of the following melting points were used: 230° C., 250° C., 285° C., 327° C.

The bases of the HC-(XM-3)/U holders were prepared so that at various locations along the height of the two Kovar pins, transverse wires of .009" diameter nickel or .007" phosphor-bronze were welded in place.

Since the heat is supplied through an R-F induction coil, it is desirable to keep the amount of metal that cuts through the lines of magnetic flux to a minimum.

Any metal members that are in this field should be discontinuous. As a result, these transverse wires were cut, after welding to the Kovar pins, to eliminate closed loop magnetic circuits.

6.2. HC-(XM-3)/U Holder (Continued)

The effect of a cooled split copper heat sink in contact with that portion of Kovar pin outside the enclosure was not successful. This extra amount of metal tended to heat the Kovar pins more, causing the temperature indicating solders to melt more readily.

The temperature of the Kovar pins is elevated in three ways:

- I. Induction from the energized R-F coil.
- 2. Radiation from the heated Kovar sealing ring.
- Conduction through the glass from the heated Kovar sealing ring to the Kovar pins, followed by conduction in the pin itself.

The temperature at which solders melted increased as the distance from the Kovar ring increased. This would tend to substantiate a combination of Factors 2 and 3 above.

The data taken tend to indicate that at the following heights above the plane of the Kovar ring, the following solders did <u>not</u> melt.

Distance Above Kovar Ring	Solder
3/8"	-327 ° C.
1/2"	-285° C.
- 113 -	-250 ° C.

6.2. HO-(XM-3)/U Holder (Continued)

Arrangements were made with Reeves-Hoffman Division of Dynamics Corporation Of America, Carlisle, Pennsylvania, to attempt to mount CR-38/U crystals of the following frequencies: 24, 36, 51, and 100 Kc. The solders to be used were 280° C., 292° C., and 315° C. Although this manufacturer modified the standard procedures used to fabricate crystals of this type, the attempts to satisfactorily mount crystals were unsuccessful. The report of this work follows:

"SUBJECT: Reeves-Hoffman Division Project C-9413
for Corning Glass Works. Process 24, 36,
51 and 100 Kc. CR-38/U crystals using
high temperature solder, to be mounted on
special glass header and envelope supplied
by Corning Glass Works.

"ABSTRACT

"The attempt to fabricate a crystal for mounting in HC-(XM-3)/U holder for Corning Glass Works has not been successful. The solders requiring temperature of about 300° C. are required to withstand the heat necessary to seal the envelope lead attachment employing these solders achieve a bond of insufficient strength to withstand the forces encountered in fabricating the unit for mounting.

6.2. HC-(XM-3)/U Holder (Continued)

"ABSTRACT (Continued)

"The crystals were prepared by standard procedures summarized as follows:

Cut: NT

Surface Finish: 12.5 Micron Abrasive

Etch: NH4: FHF, 50° C., 105 sec.

Spot: At nodal point, Hanovia liquid silver

No. 150, .042 inch diameter, ca .0002

inch thick fired at 550° C.

Gold Plate: Sputtered 25 min.

125 ma. at 50 microns of Hg

"The following are the phases of crystal finishing accomplished.

"LEAD PREPARATION

"Gold plated, phosphor bronze (ASTM Alloy C) headed wires, .0063 inches in diameter were employed.

"The head of the wire was 'tinned' about .025 inches by immersing in molten solder of the alloy to be used for the lead attachment.

"Solder spheres, .018 inch diameter, were attached to the 'tinned" portion of the wire. The spheres were melted in molten stearine flux.

6.2. HC-(XM-3)/U Holder (Continued)
"LEAD PREPARATION (Continued)

"The stearine flux quickly boiled away and required constant replacement. The vapors were very annoying and on occasion became hot enough to ignite.

"The spheres melting at 280° C. were the most difficult to place on the wires. The least difficulty was encountered with those melting at 292° C.

"All leads required three rinses in trichlorethylene to remove oxidized flux.

"The chromed dish for pellet placement was cleaned by an overnight soak in Oakite Rustripper.

"The following temperatures were required of the hot plate to prepare the leads:

Melting Point Of Solder Temperature Used 280° C. 320° C. 292° C. 330° C. 315° C. 355° C.

6.2. HC-(XM-3)/U Holder (Continued)

"LEAD PREPARATION (Continued)

"The following solders were supplied by Corning Glass Works:

Alloy No.	Indium	Lead	Silver	Melting Point
83	5	92.5	2.5	280 - 285° C.
87	5	95	-	315° C.
88	5	90	5	292° C.

"LEAD ATTACHING

"The thermostat of the platen of the lead attach machine was disconnected and the temperature controlled by adjusting the variac.

"The following temperatures were measured:

Platen: ca 500° F. (260° C.)

Air Blast: ca 740° F. (393° C.)

"The rosin-alcohol flux normally used did not cause the solder to flow.

"A flux of the zinc chloride in water type

(Nalco 14) was necessary. The high temperature
caused the water to boil with much vigor leaving
a residue of zinc chloride which readily
charred. The burned residue contaminated the work
surface making the operation extremely difficult.

6.2. HC-(XM-3)/U Holder (Continued)

"LEAD ATTACHING (Continued)

"A lead was attached, the crystal washed in distilled water, dried, and returned to the platen for the opposite lead.

"A final cleaning in boiling distilled water was used to remove all traces of flux.

"The appearance of the solder cone did not conform to R-H standards.

"The holding jaws of the lead attach machine were removed and the entire working surface cleaned with cleaner and steel wool.

"PRIMARY FREQUENCY ADJUSTMENT

"The crystals were suspended between spring loaded jaws connected to an oscillator. The lead attachment of 10% of the units failed to withstand this handling.

"BENDING THE LEADS FOR MOUNTING

"The lead attachment of all remaining crystals failed to withstand the handling necessary to bend the wire preparatory to mounting.

6.2. HC-(XM-3)/U Holder (Continued)

"BENDING THE LEADS FOR MOUNTING (Continued)

"The tensil strength of the lead attachment was considerably less than is obtained with eutectic solders and rosin flux.

"WEIGHT ATTACHMENT

"Attempts were made to place dampening weights on the wires. (Weight 38 mg., M.P. 292° C.)

"The soldering tool was heated in excess of 320° C.

The pellets placed in stearine palmoil flux.

"The usual procedure of rolling a molten pellet down the soldering iron was tried.

"A zinc chloride flux (Kester 714) was first applied to the wire.

"The iron did not impart sufficient energy to the solder for it to properly adhere on the wire.

"ADAPTING MICA SPACER TO ENVELOPE

"Mica spacers (Reeves-Hoffman Part C-1067) with two nickel eyelets were resized to fit the glass envelope.

6.2. HO-(XM-3)/U Holder (Continued)

"ADAPTING MICA SPACER TO ENVELOPE

"A No. 600 abrasive paper was used to remove the excess mica. Abrading continued until the mica was reduced to size sufficient to fit the glass.

"The mica is intended to restrict the heat of sealing, thereby protecting the crystal."

Since conventional mounting techniques of quartz units for this holder type were not compatible with the temperature attained during sealing, contract modifications were made. These changes stipulated that pre-production test samples were to be sealed in the same manner as were HC-(XM-2)/U holders but without any quartz blanks, and subjected to the specified environmental tests.

Bulbs of 7052 glass and bases made of 7052 CLEARFORM^(R)
parts were subject to pre-production testing.

Environmental tests were passed and the pilot production was completed.

6.3. <u>HC-(XM-4)/U Holder</u>

The initial design of this holder followed very closely that of the Philips RG-2 holder. The Government owned sealing equipment located at McCoy Electronics, Mount Holly Springs, Pennsylvania, was used for initial sealing experimentation. The first sealing attempt was not successful but it demonstrated the need for a good fit between the bulb and the base as well as the need for uniformity of bulb wall thickness in the sealing area. This initial sealing work, even though not successful, indicated that quartz crystal temperatures would be near or greater than the 250° C. maximum stipulated.

After several changes in bulb and base design specifications, units were capable of being successfully sealed. When successful seals were made, the 250° C. limit as measured with solders was exceeded. Accordingly, pre-production samples were made incorporating quartz crystals of frequencies 10 and 75 Mc. Frequency and resistance values before and after sealing are tabulated. No particular attempts were made to produce an exact frequency. The use of quartz crystals demonstrated that good units can be sealed in glass holders.

6.3. HC-(XM-4)/U Holder (Continued)

		nominal)	Frequency	(of	tance
Nominal	Before	After	Change	Before	After
Frequency	Seal	Seal .	(ppm)	_Seal_	Seal
75 Mc	- 580	+ 370	+12.7	39	32
**	-410	+1246	+22.1	55	1246
11	-432	- 893	- 6.1	38	33
11	+740	+1618	+11.7	33	27
H	-475	+ 818	+17.3	35	27
11	-582	+ 50	+ 8.4	48	39
11	- 777	+ 551	+17.7	36	28
11	-82 6	+ 106	+12.4	33	27
Ħ	-445	1 222	+ 8.9	33	26
n	-105	+ 807	+12.2	3 6	32
**	-515	+ 488	+13.4	36	31
**	-417	+ 991	+18.8	34	26
IO Mc	+ 96	- 220	-3 1.6	22	12
11	+105	- 290	-39.5	21	10
11	+197	- 47	-24.4	21	12
11	+ 84	+ 7	- 7.7	24	14
**	+212	+ 34	-17.8	23	14
11	- 33	+ 4	+ 3.7	24	13
Ħ	+ 34	- 205	-23.9	22	14
**	+ 47	- 59	-10.6	33	10
11	+206	- 240	-44.6	25	12
11	+ 54	- 2 05	-25.9	29	14
11	- 64	- 130	- 6.6	31	16
If	+108	Inactive	- · -	30	-

These sealed units were subjected to the environmental testing phase. Units were accepted. Pilot production was completed.

7. CONCLUSIONS AND RECOMMENDATIONS

7.1. <u>HC-(XM-2)/U Holder</u>

Although the desired 250° C. maximum quartz temperature was exceeded, it was demonstrated that good quartz crystals with frequencies as low as 2.85 Mc can be satisfactorily sealed in this glass holder of the design and materials specified by the Government in Section 4. above. The length of the bulb used for the pre-production tests yielded sealed holders on the short side of the finished specification. It is suggested that subsequent bulbs be made longer to provide greater space within the holder and still be compatible with the finished holder specification. The Corning bulb specification accompanying this report shows this suggested length dimension of .705°.

Base forming experience by Tronex, since the completion of the pre-production tests and pilot run, suggest that less expensive base production will be achieved through two modifications:

- a. Remove the recess or counterbore around the Kovar pin at the outside surface of the base.
- b. Eliminate the need for glazing the Kovar sealing ring.

Neither of these two suggestions was tried or proven under the work of this contract.

7. CONCLUSIONS AND RECOMMENDATIONS (Continued)

7.2. HC-(XM-3)/U Holder

To this writer's knowledge, there is no crystal unit that is currently enclosed in a HC-13/U holder that can be encapsulated in this glass holder. Accordingly, crystals and crystal mounting techniques must be developed if units meeting the pertinent requirements of Section 4, above are to be met.

The possibility exists that lower sealing temperatures might be achieved using materials other than those specified in the original requirements of this contract. The use of alternate or additional materials would tend to complicate an already compromised sealing technique. However, in any hermetic sealing system, it is usually desirable and advantageous to keep the system as simple as possible; that is, avoid introducing dissimilar materials that have differing thermal coefficients of expansion or different viscosity characteristics.

Since the sealing method for the HC-(XM-3)/U and HC-(XM-2)/U holders are the same, any reduction of sealing temperature for one would be applicable for the other.

Base forming experience by Tronex, since the completion of the pre-production tests and pilot run, suggest that

7. CONCLUSIONS AND RECOMMENDATIONS (Continued)

7.2. HC-(XM-3)/U Holder (Continued)

less expensive base production will be achieved through two modifications:

- a. Remove the recess or counterbore around the Kovar pin at the outside surface of the base.
- b. Eliminate the need for glazing the Kovar sealing ring.

Neither of these two suggestions has been tried or proven under the work of this contract.

7. CONCLUSIONS AND RECOMMENDATIONS (Continued)

7.3. HC-(XM-4)/U Holder

The desired temperature of 250° C. was exceeded, but it was satisfactorily demonstrated that good quartz crystals with frequencies as low as 10 Mc can be sealed in this glass holder.

Bulb forming experience, since the completion of the pre-production tests and pilot run, suggest that less expensive bulb production will be achieved if the overall length of the bulb is changed from 2.031" to 1.500", or shorter. Such a change may require that sealing equipment be modified.

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 Corporation, Limited, Toronto, Ontario, CANADA, (Now

 known as Philips Electronics Industries, Limited)

9. ACKNOWLEDGMENTS

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Isotronics, Inc., and L. L. Constantin And Company,
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Reeves-Hoffman Division Of Dynamics Corporation Of
America, Carlisle, Pennsylvania

Scientific Radio Products, Inc., Loveland, Colorado Tronex, Inc., Millville, New Jersey

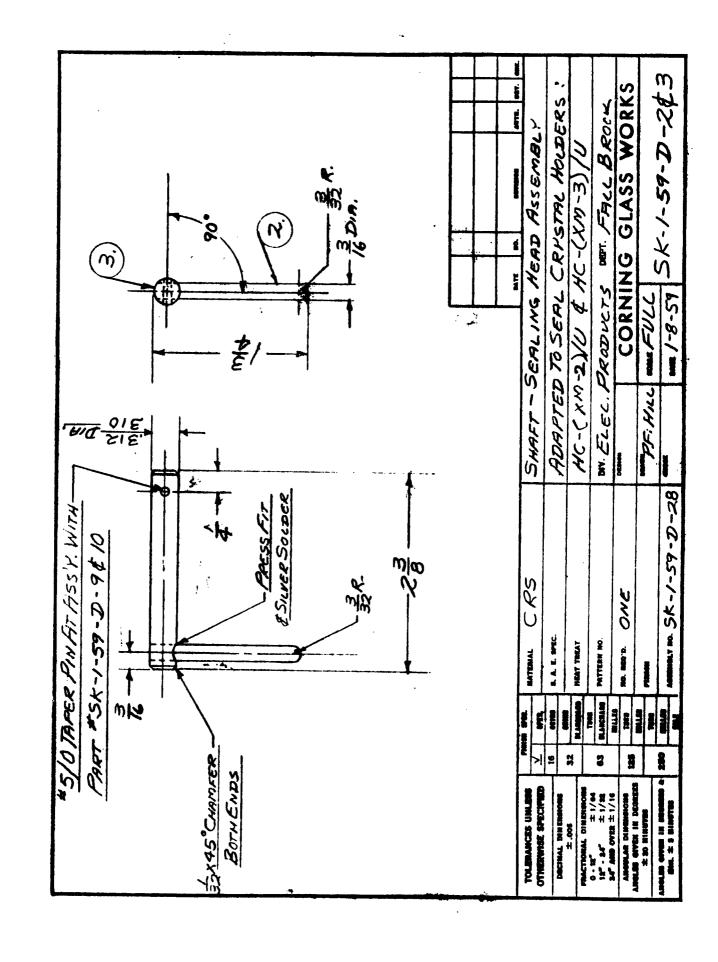
(United States Army Signal Supply Agency) now called:
United States Army Electronic Materiel Agency,
Philadelphia, Pennsylvania

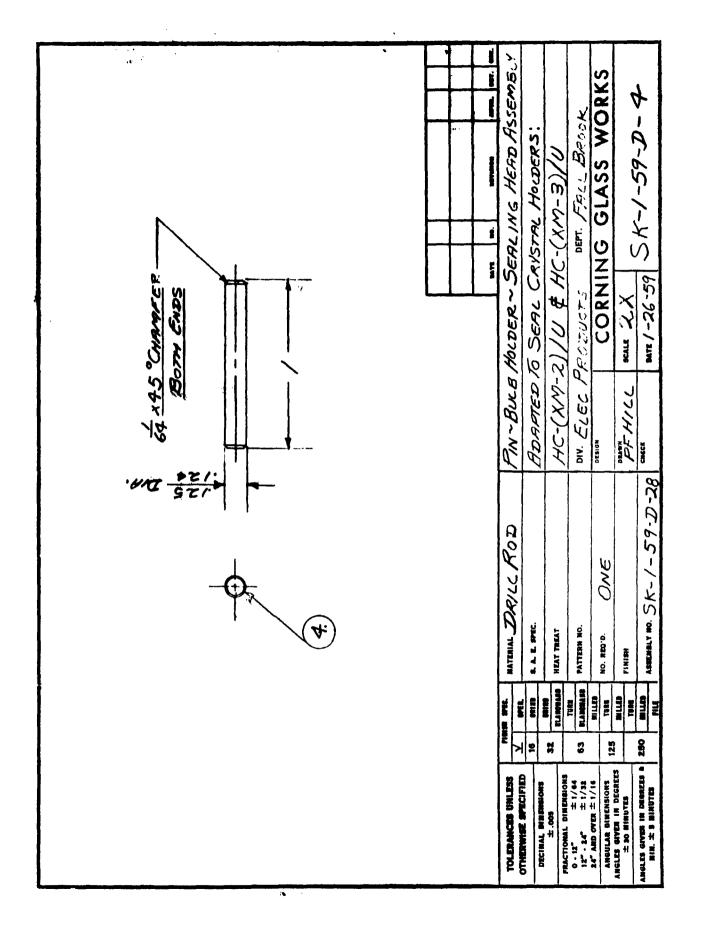
(United States Army Signal Equipment Support Agency)
now called: United States Army Signal Materiel
Support Agency, Fort Monmouth, New Jersey

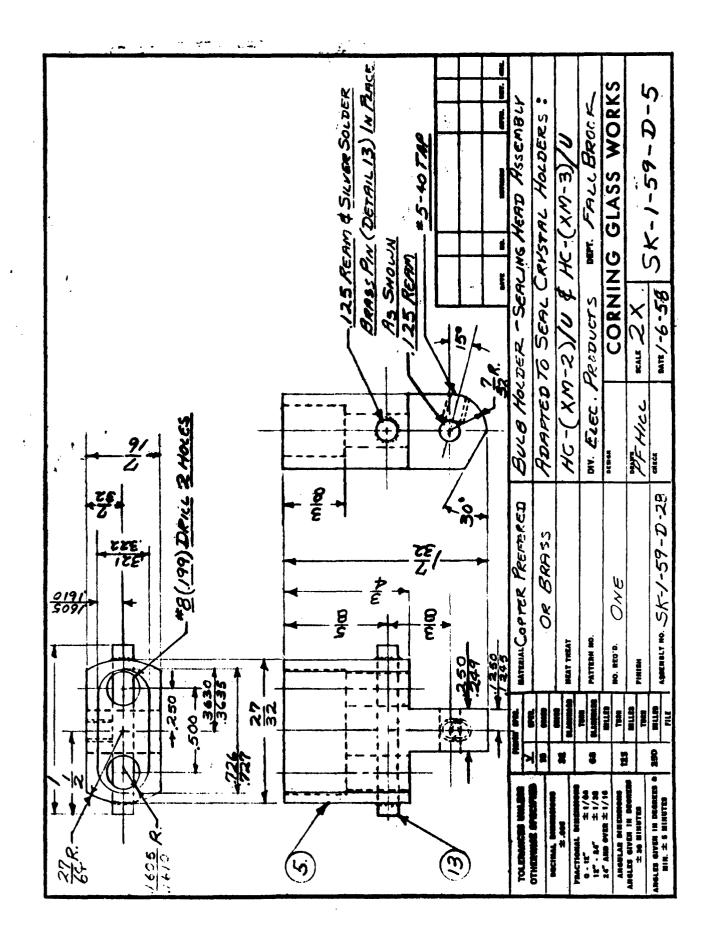
APPENDIX

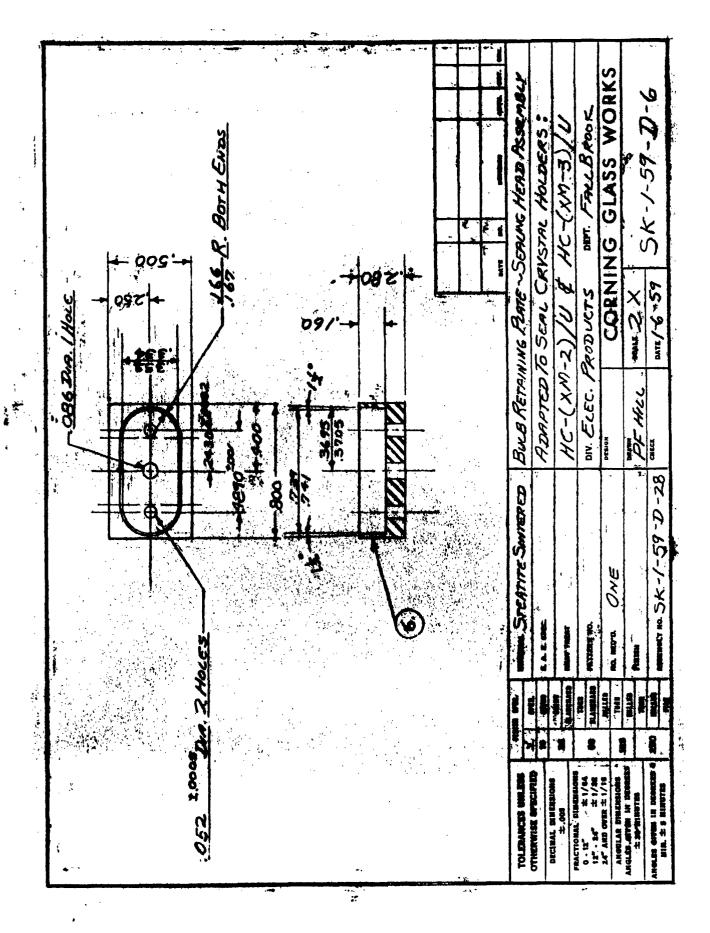
On the following pages are detail drawings of the Corning modifications of the sealing head. These modifications allow both the HC-(XM-2)/U and HC-(XM-3)/U holders to be sealed on the same machine.

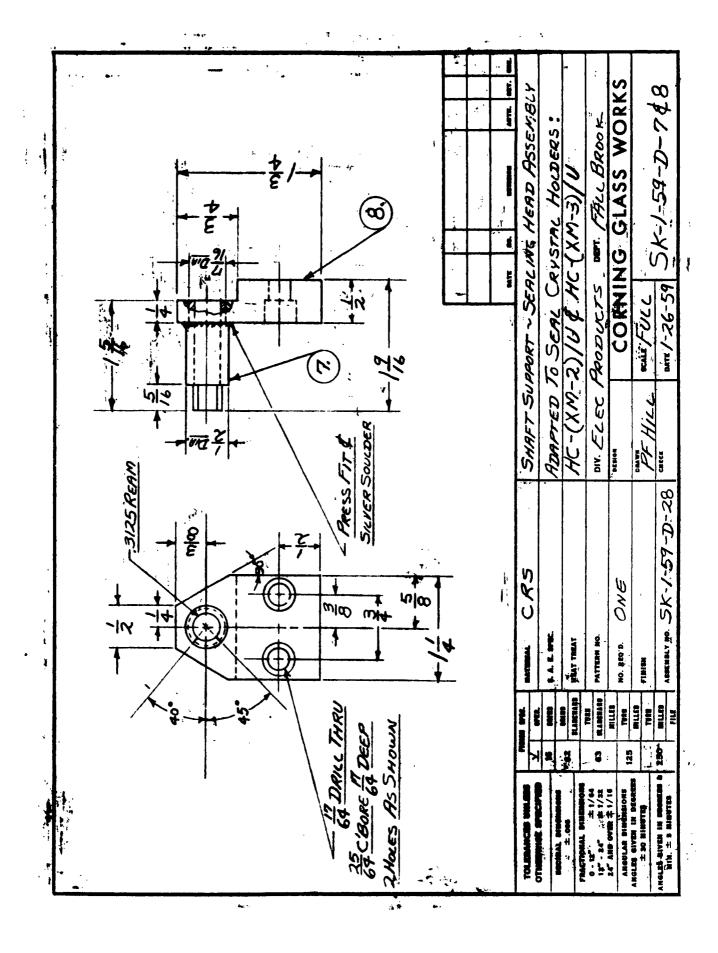
CORNING GLASS WORKS MACHINE PARTS LIST DWG. JOB NO.SK-1-59-D-28 DIV ELECTRICAL PRODUCTS PLANT Fall Prook DEPT Equipment Engineering TITLE COMPILED BY P. P. Hill SHEET NO. I SEALING HEAD ADAPTED FOR SEALING 1/7/58 NO. SHEETS CRYSTAL HOLDERS: HC-(XM-2)/U & HC-(XM-3)/U I REQ'D NAME PART AND DWG. NO. PATT, NO. MATERIAL SK-1*59*D-28 Ass'y Sealing Head SK-1-59-D - 1 2 1/4-20 Socket Head Cap Screw - 5/8 long Purchase 1 2 C.R.S. Shaft 3/16 diameter 3 1 H 5/16 H 1 1/8 diameter pin Drill Rod 5 1 Copper Bulb Holder 6 Steatite Retaining Plate 7 1 C.R.S Shaft Support 8, 1 C.R.S. 9 1 Drill Rod Lift Wheel: 10 1 C.R.S. . . 11 1 Spring Holder 12 1 Brass Collar 13 1 Pin 1 14 Steatite Locating Plate 15 Brass Nut____ 16 1 Locating Plate Holder 17 1 Drill Rod Spring Holder 18 Music Wire Estension Spring 19 1 C.R.S. Support Pin 20 1 Brase Housing____ 21 1 Music Wire Compression Spring 22 C.R.S. Housing Base . 23 1 Bronze Bushing ٠1 #5-40 Set Screw 3/16 Tong 24 Purchase 1 25 C.R.S. Sealing Head Holder 26 1 Pyrex Glass Bell Jan 27 Copper Adaptor - Bulb Holder 28 Assembly Drawing

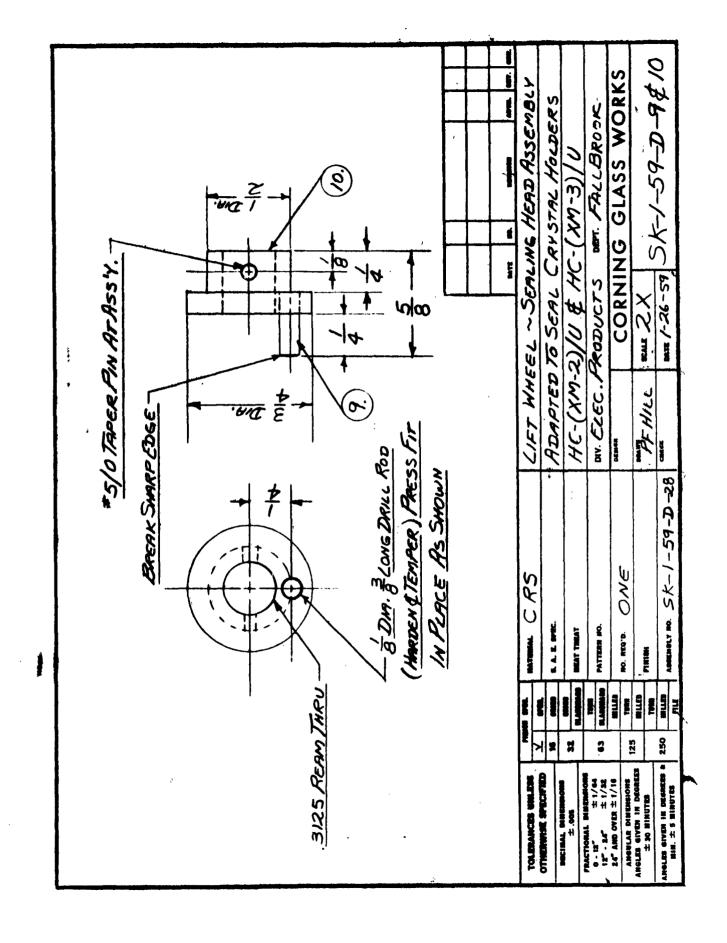


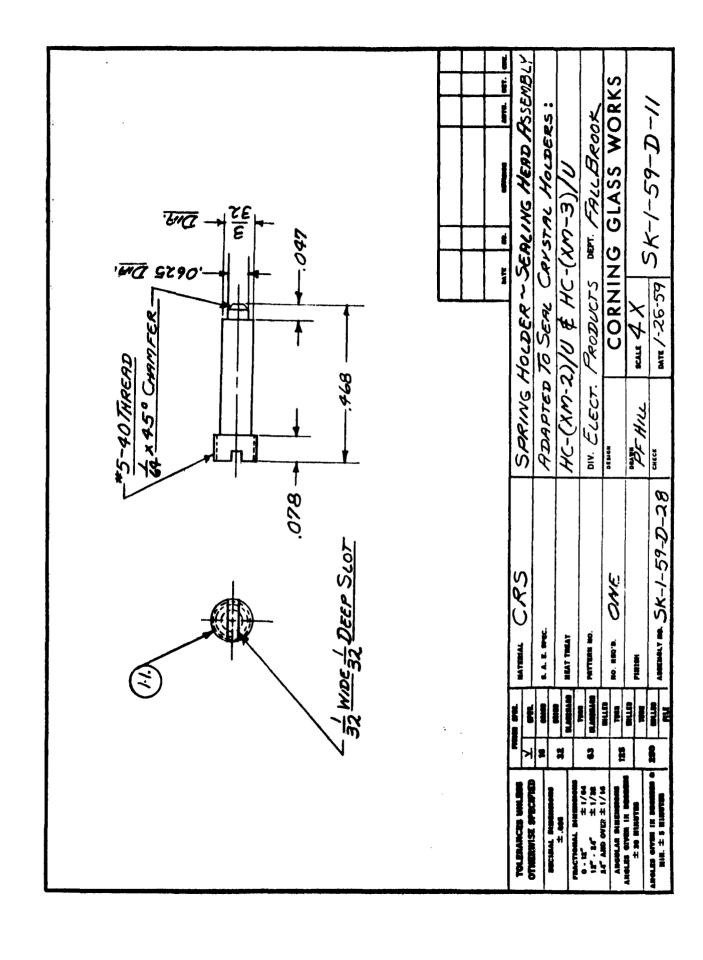


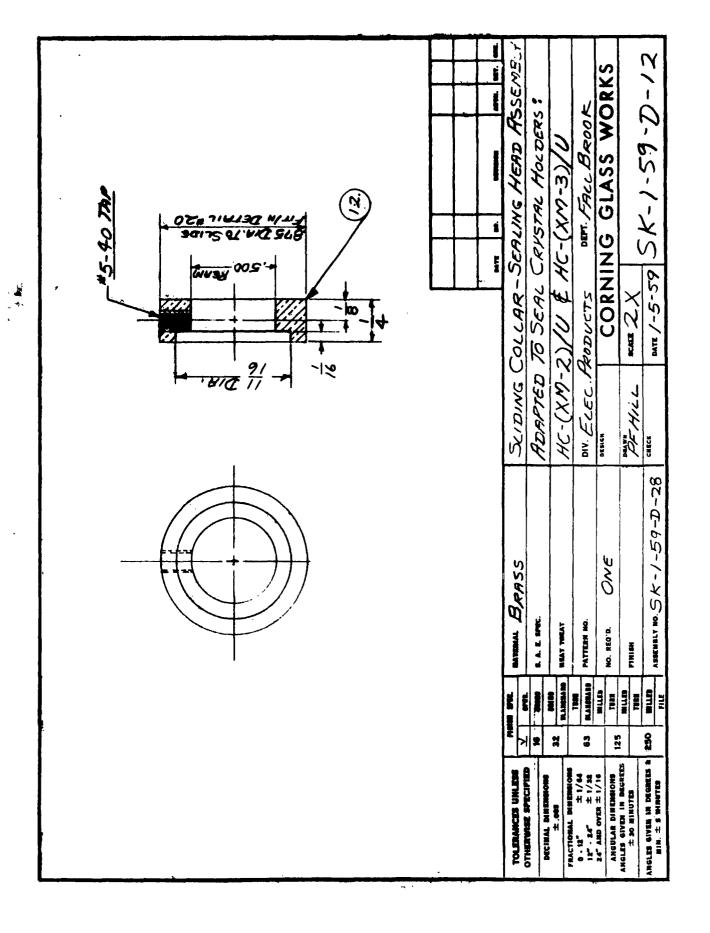


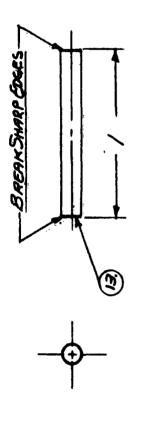












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